

*i3C Symposium  
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**Structural behaviour of flexible pavements  
under seasonal moisture variations and  
frost/thaw conditions**

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Sweden

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# Overview

## 1. Background

## 2. Full Scale Accelerated Pavement Testing (APT)

APT – HVS test results showing moisture dependency on the behaviour on unbound layers and subgrades.

## 3. Laboratory Experiments

Stiffness and accumulation of permanent deformation – observed behaviour and modelling.

## 4. Full Scale Field Monitoring and Back-Calculation

Moisture in pavement structures and its influence on structural response due to heavy traffic loading.

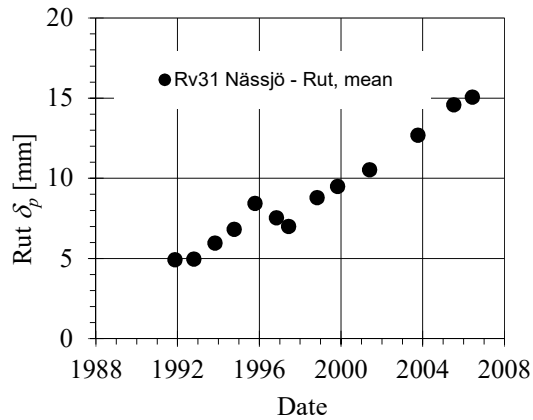
## 5. Pavement Design and Performance Prediction

## 6. Summary

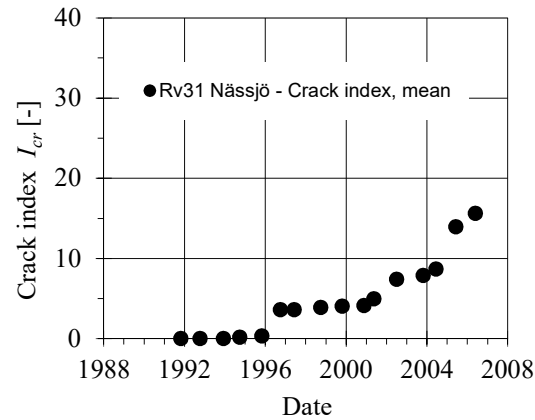
# Background #1

## Distress mechanisms

### Rutting



### Fatigue cracking



### Studded tyre wear



### Frost heave & cracking

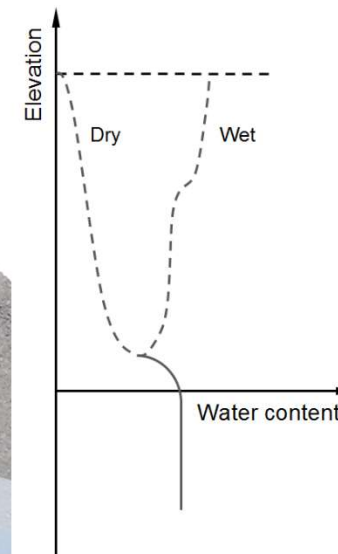
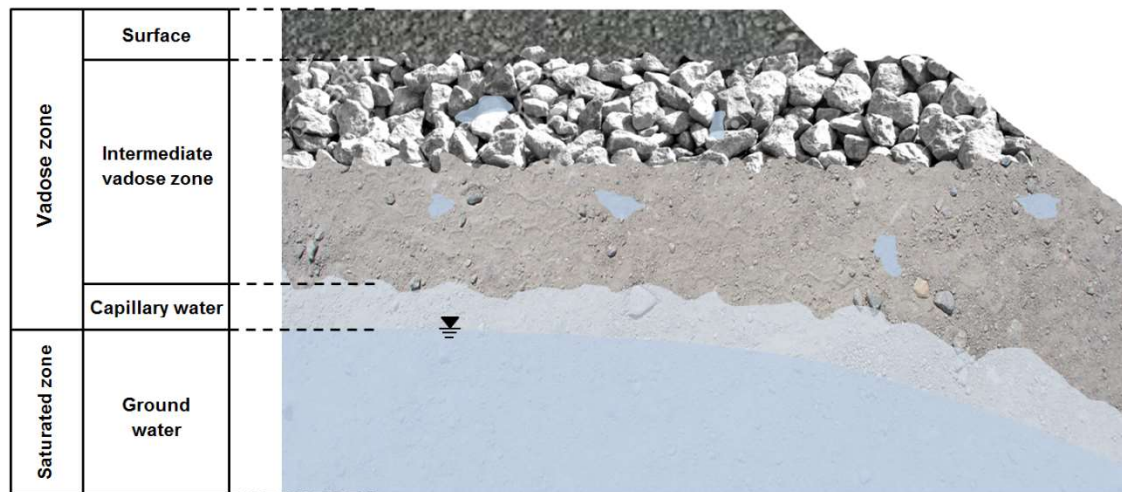


### Low temperature cracking



# Background #2

## Regions of water in pavements



### Vadose zone:

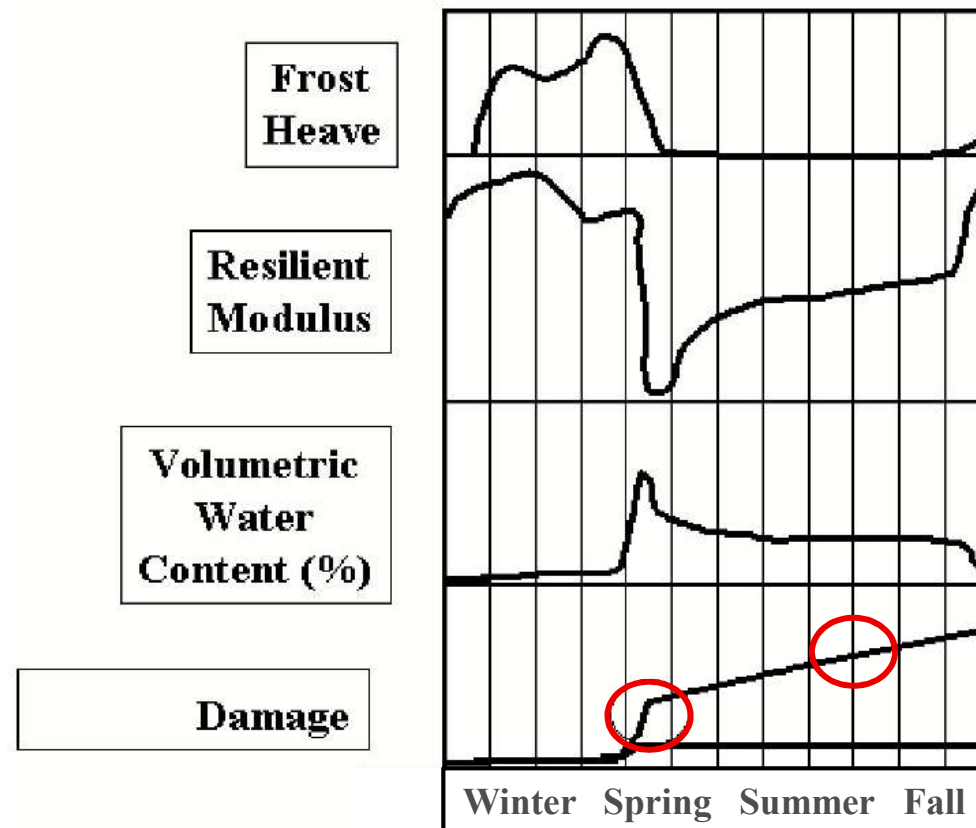
- Surface water
- Intermediate vadose zone
- Capillary water

### Saturated zone

- Groundwater

# Background #3

## Damage accumulation in thin flexible pavements

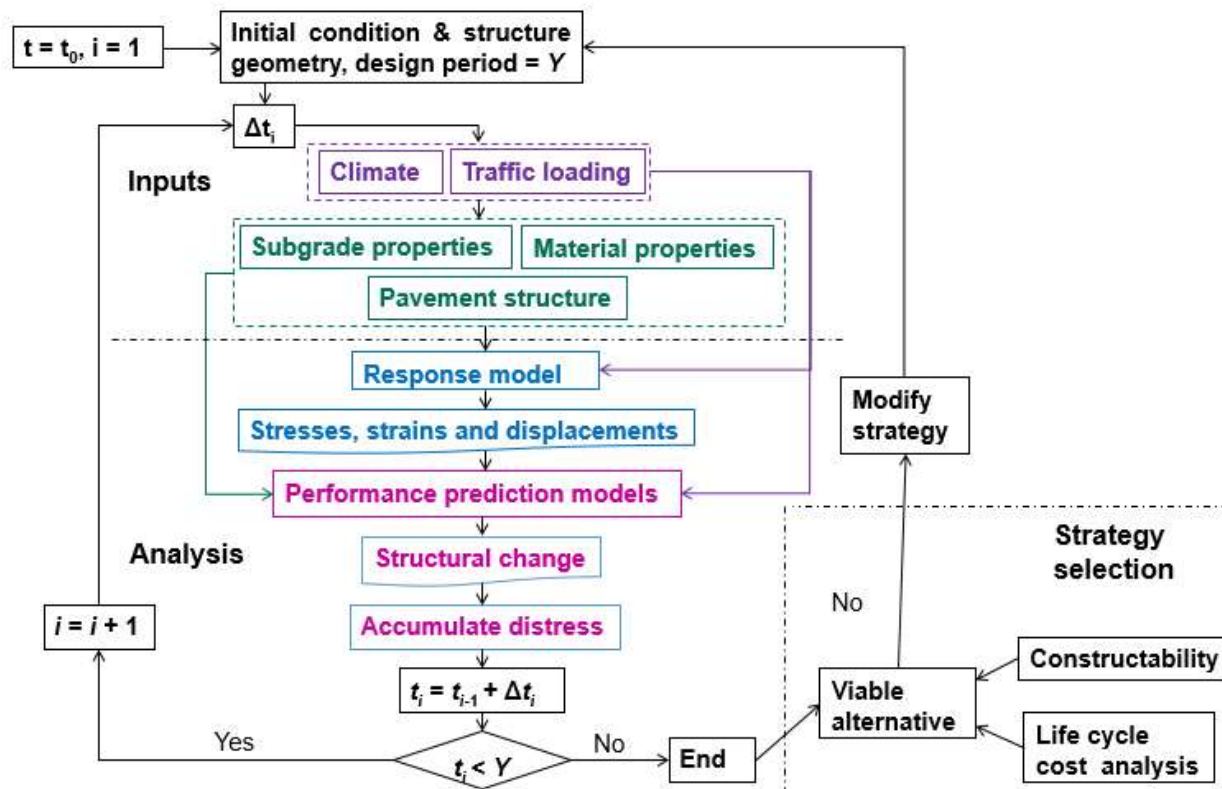


Kestler, M.A. 2003. "Techniques for Extending the Life of Low-Volume Roads in Seasonal Frost Areas". Transport Research Record 1819, Paper no. LVR8-1150.

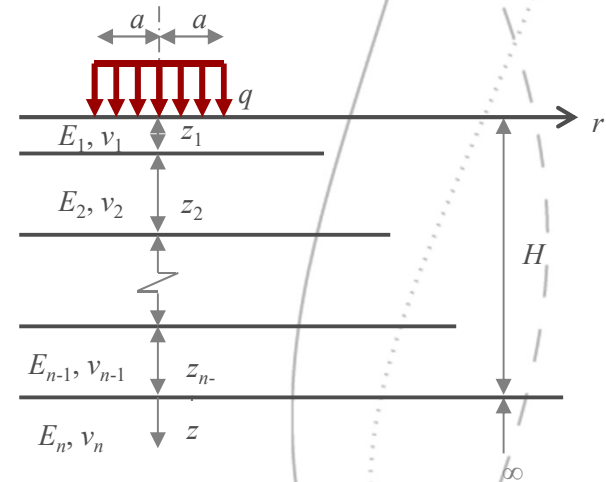
# Background #4

## M-E design ERAPave PP

### Overview

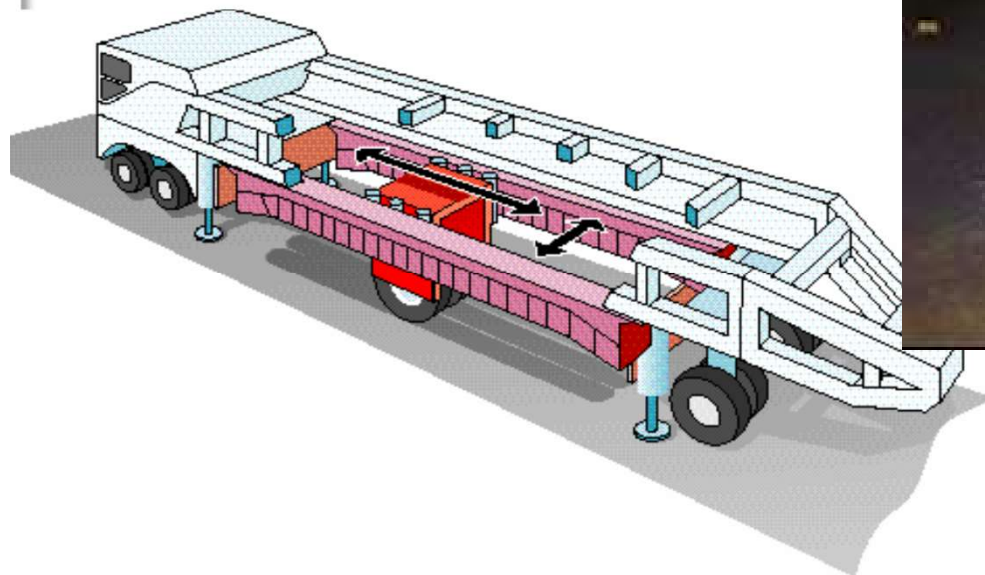


### 2D Axi sym. MLET



# APT Full Scale Testing - HVS equipment

The Heavy Vehicle Simulator (HVS) is a mobile APT test facility.

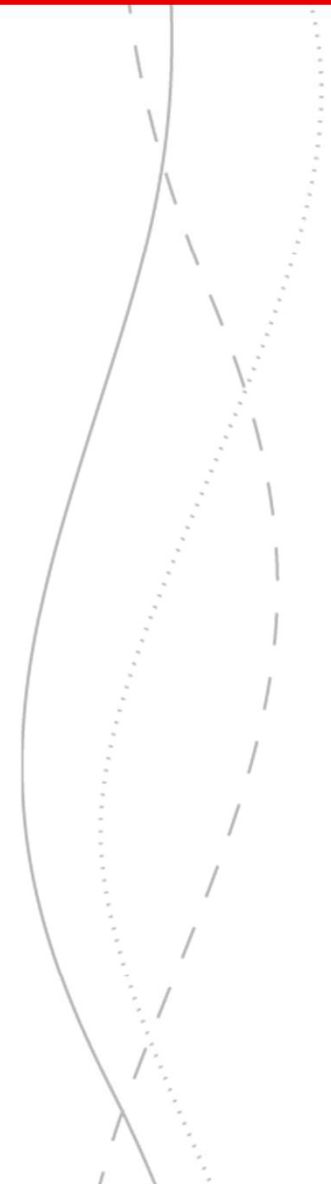


# Construction of a test object #1

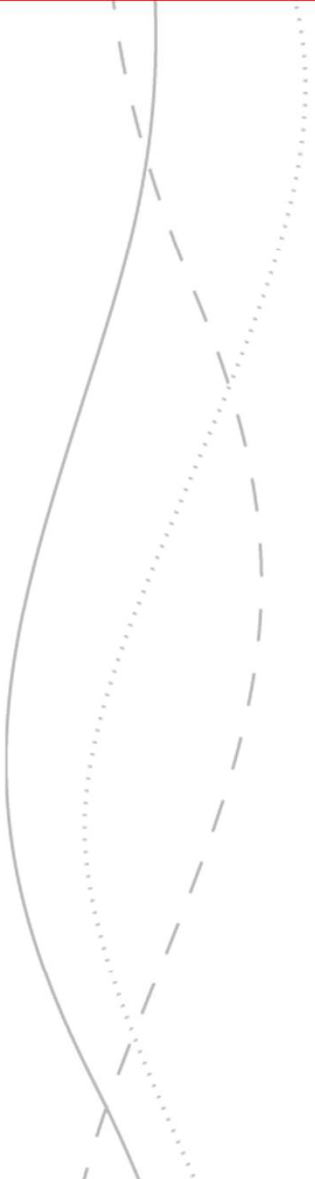




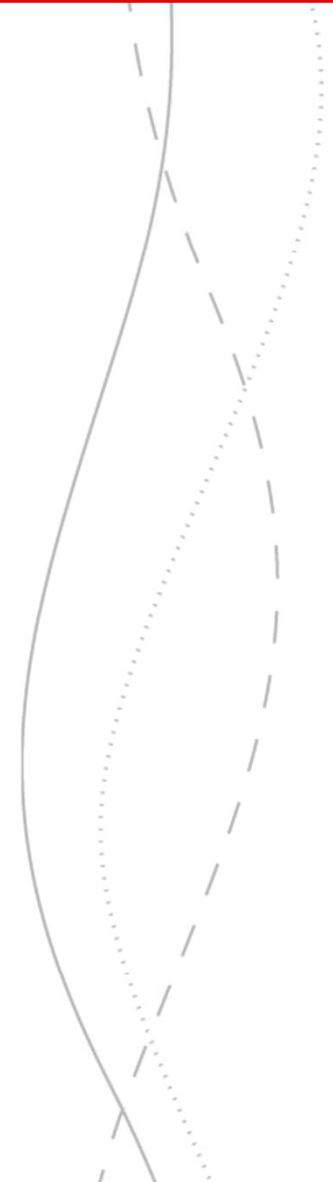
## Construction of a test object #2



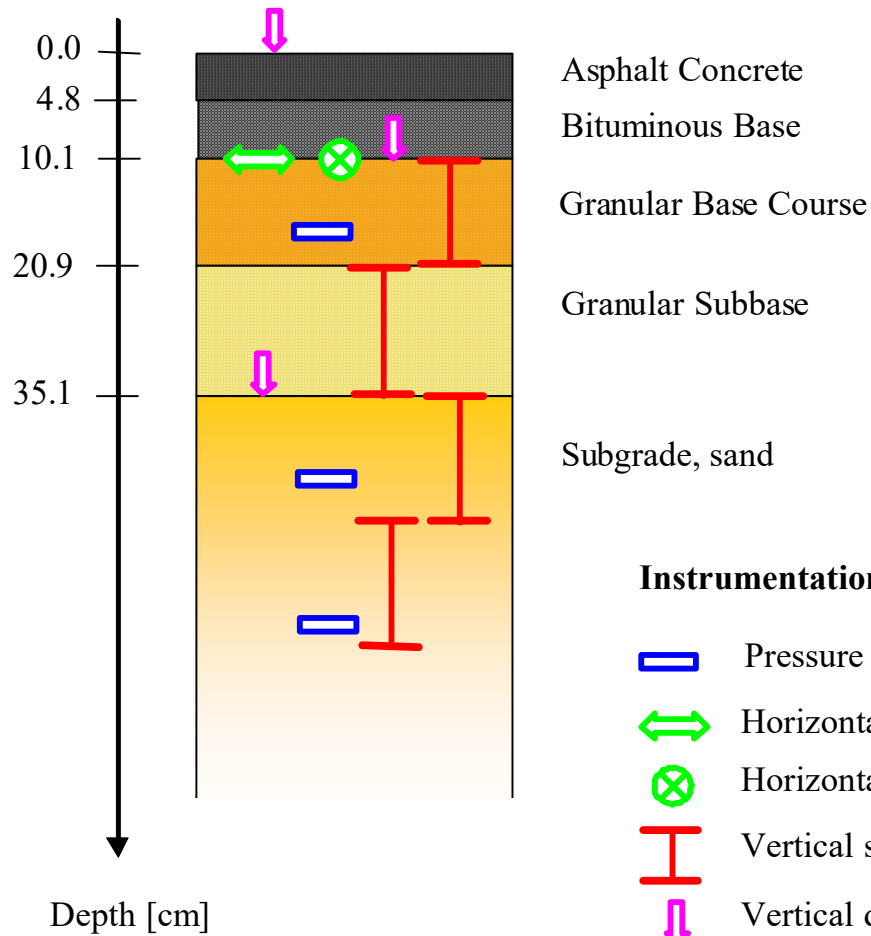
# Construction of a test object #3



## Construction of a test object #5








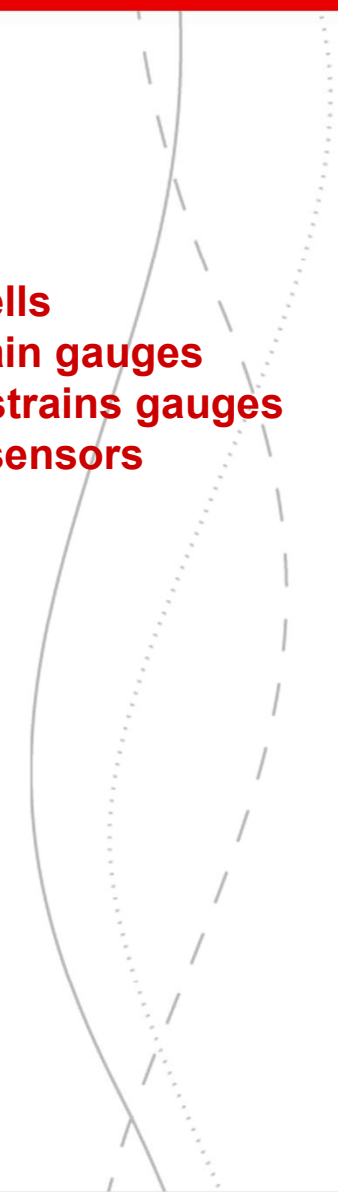
# Instrumented test structure



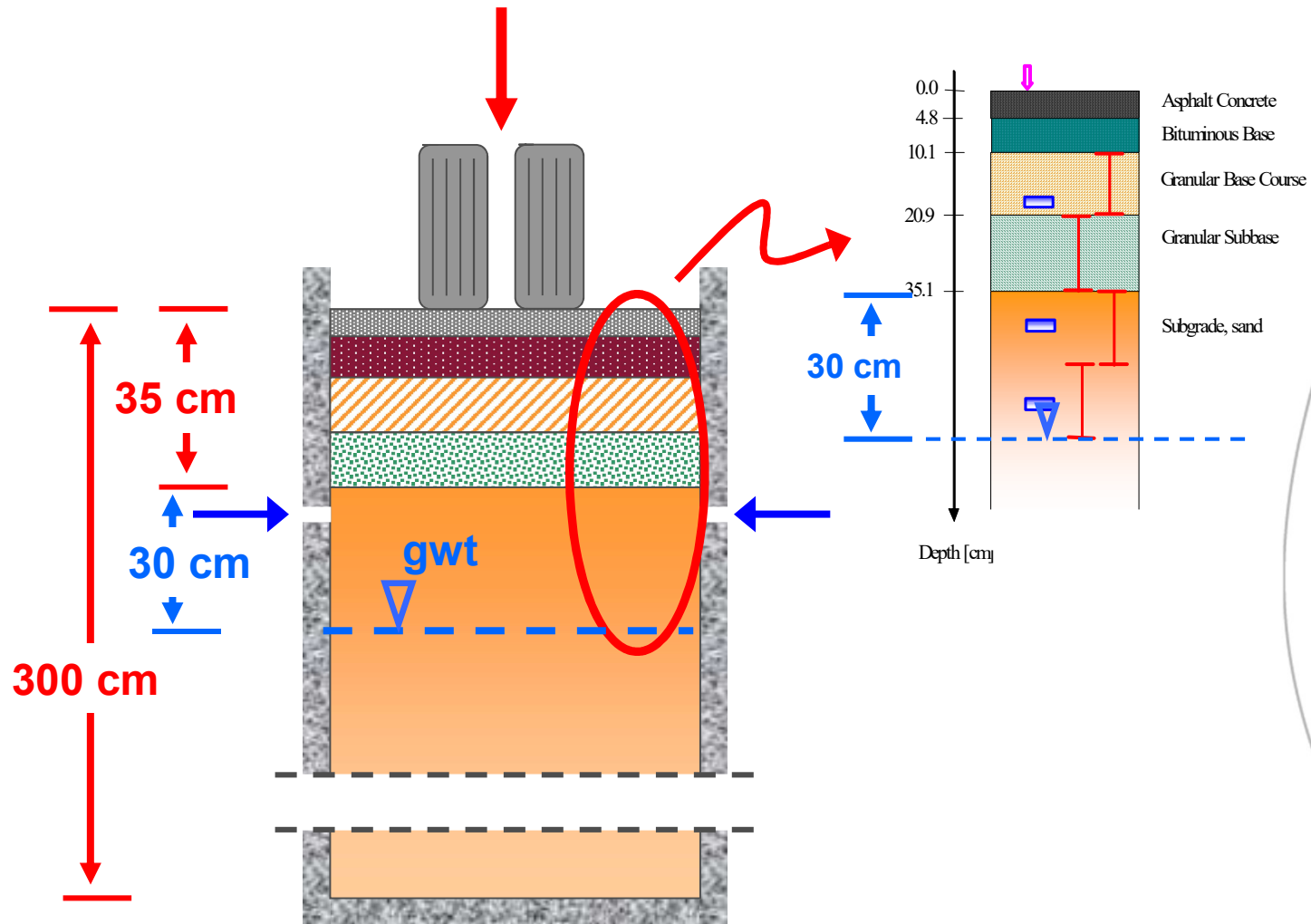
**3 x 3 Pressure cells**  
**3 x 4 Vertical strain gauges**  
**4 x 2 Horizontal strains gauges**  
**1 x 3 Deflection sensors**

### Instrumentation

-  Pressure cell
-  Horizontal strain, longitudinal
-  Horizontal strain, transversal
-  Vertical strain
-  Vertical deflection

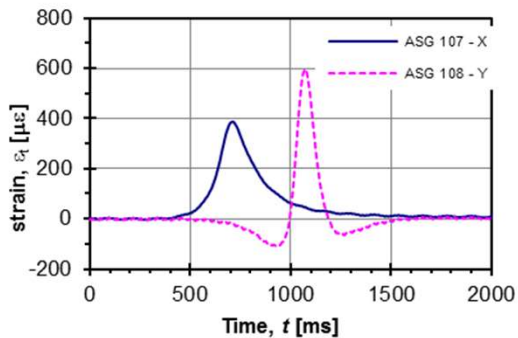


# Test procedure

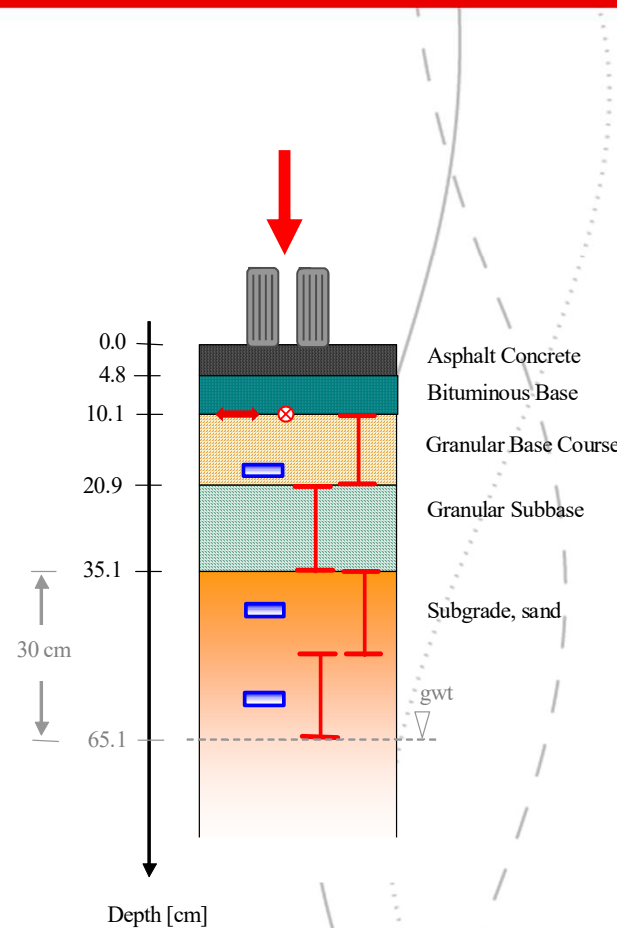
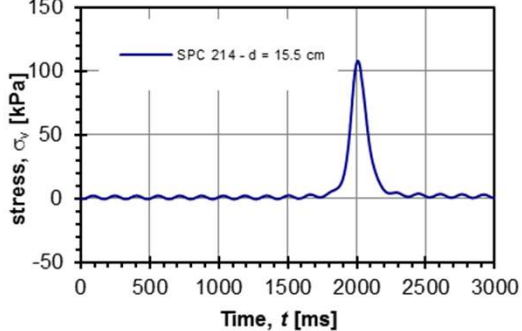
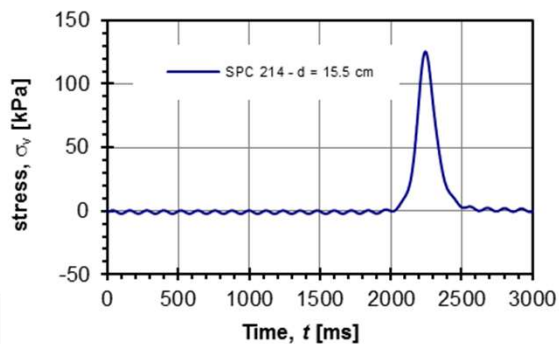
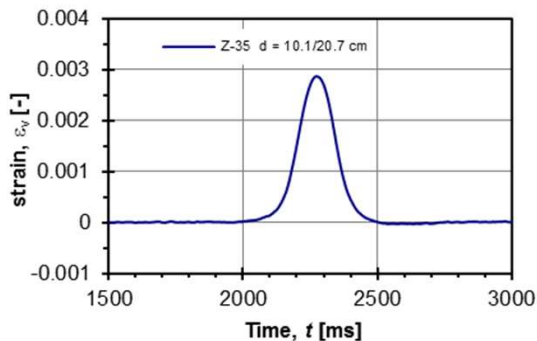
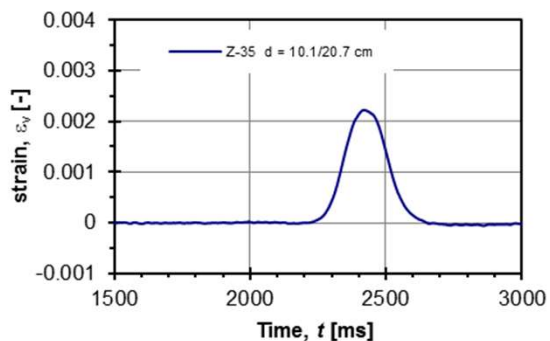
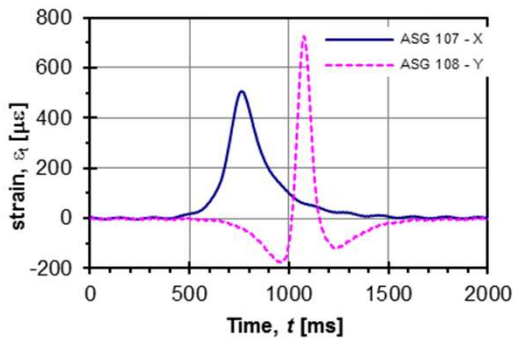


# Sensors registration

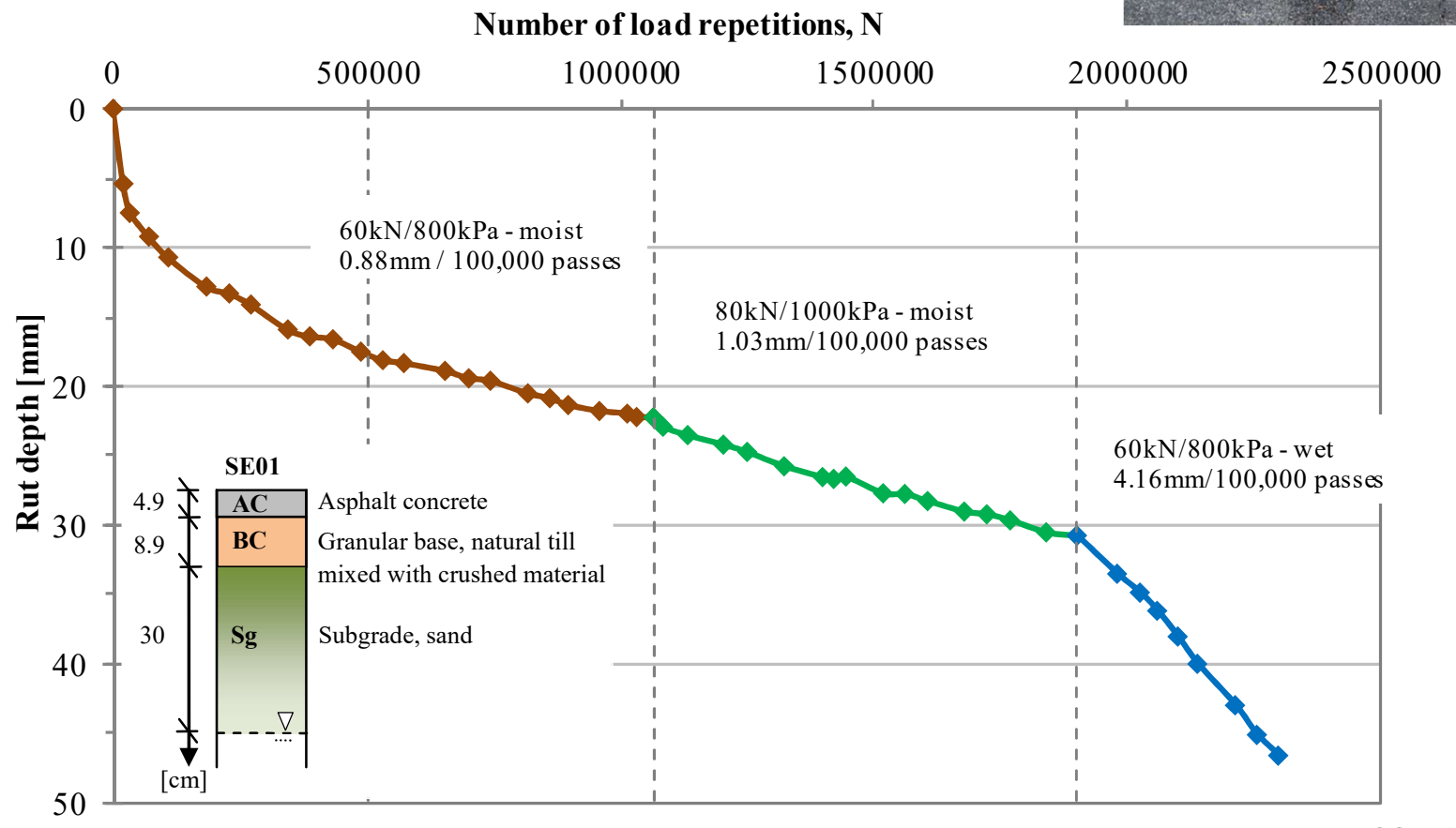
Moist



Wet



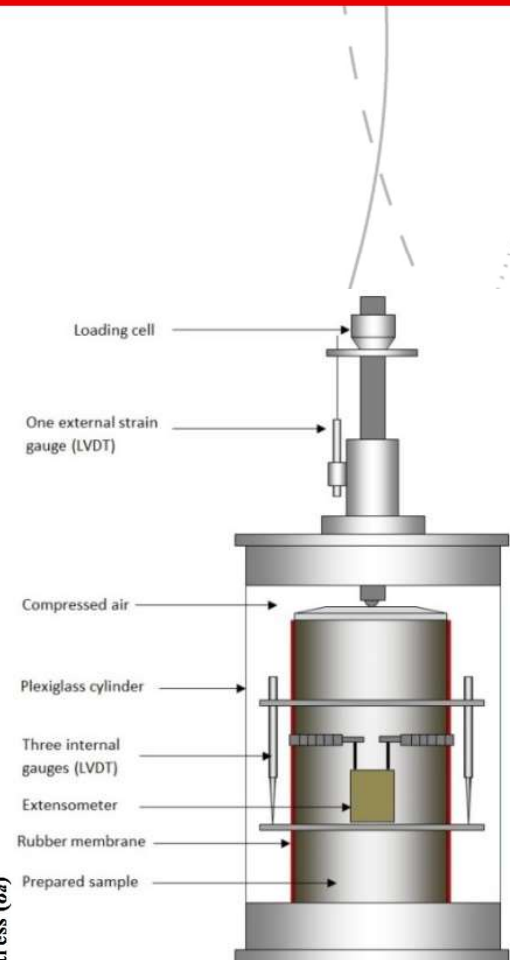
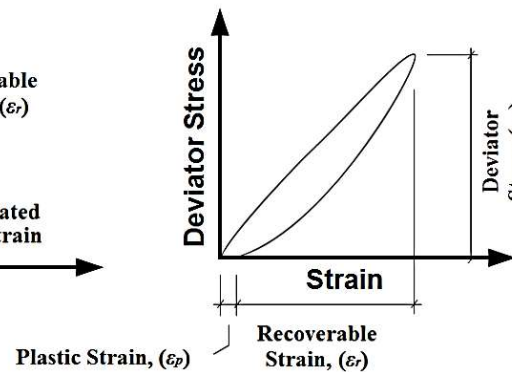
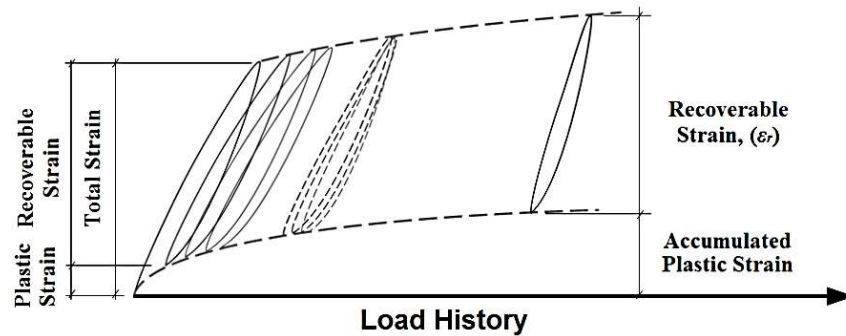
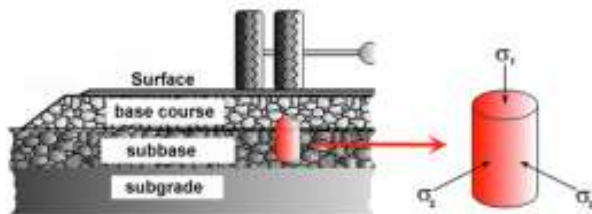
# HVS - Influence of water



# Laboratory experiments

## Stiffness and perm. deformation testing

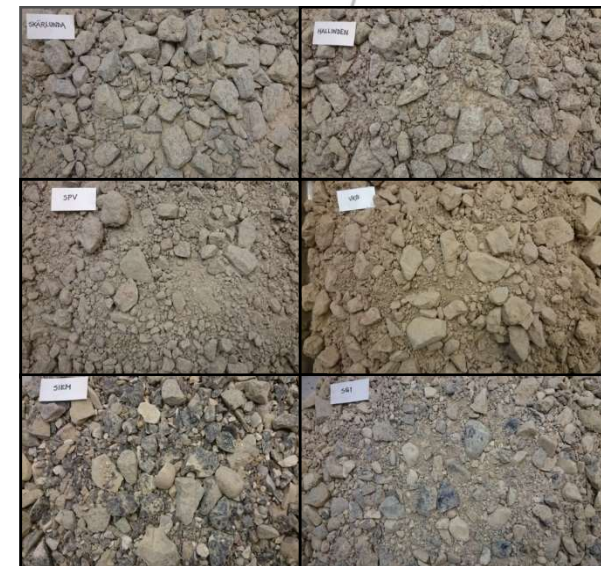
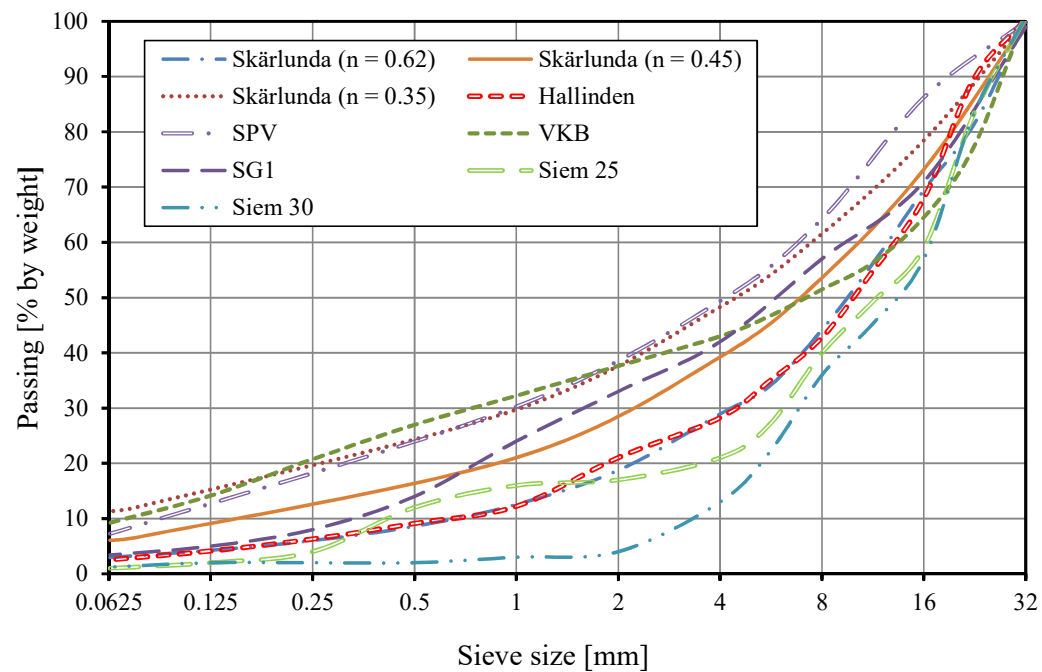
Repeated load triaxial testing





## Materials Tested

- Crushed rock aggregates and blends of natural and crushed rock
- Series of moisture contents, degree of compaction, grain size distribution

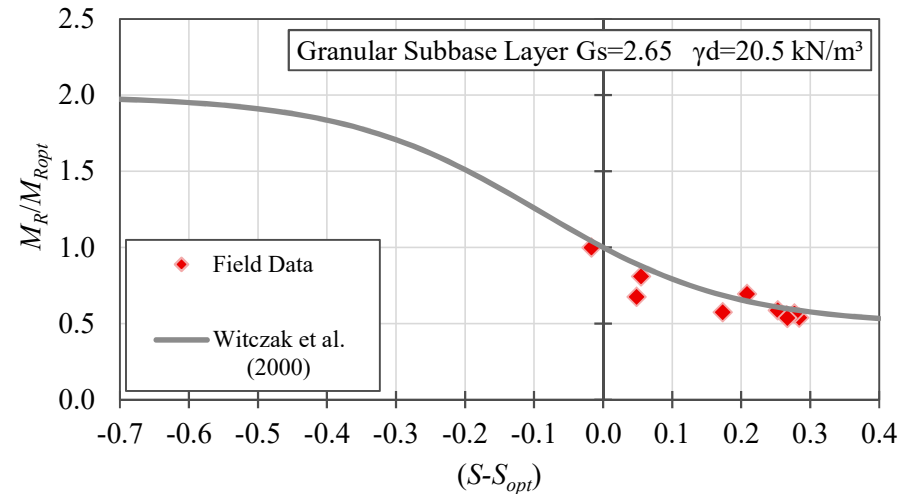
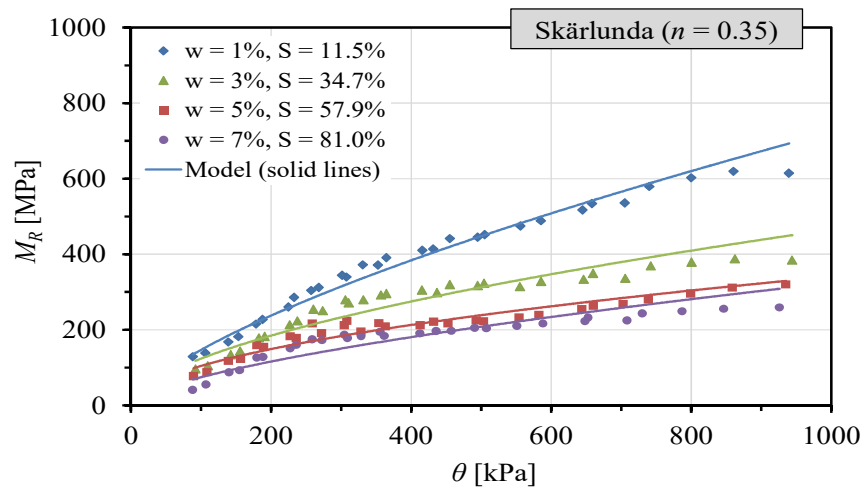


## Moisture impact on resilient deformation

- $M_R$  decreased when  $w$  increased, finer grading more affected
- The  $k$ - $\theta$  model

$$M_R = k_1 p_a \left( \frac{\theta}{p_a} \right)^{k_2} \quad k_1 = k_1(w \text{ or } S_r)$$

$$\log \frac{M_r}{M_{ropt}} = a + \frac{b - a}{1 + \exp\left(\ln \frac{-b}{a} + k_m (S - S_{opt})\right)}$$

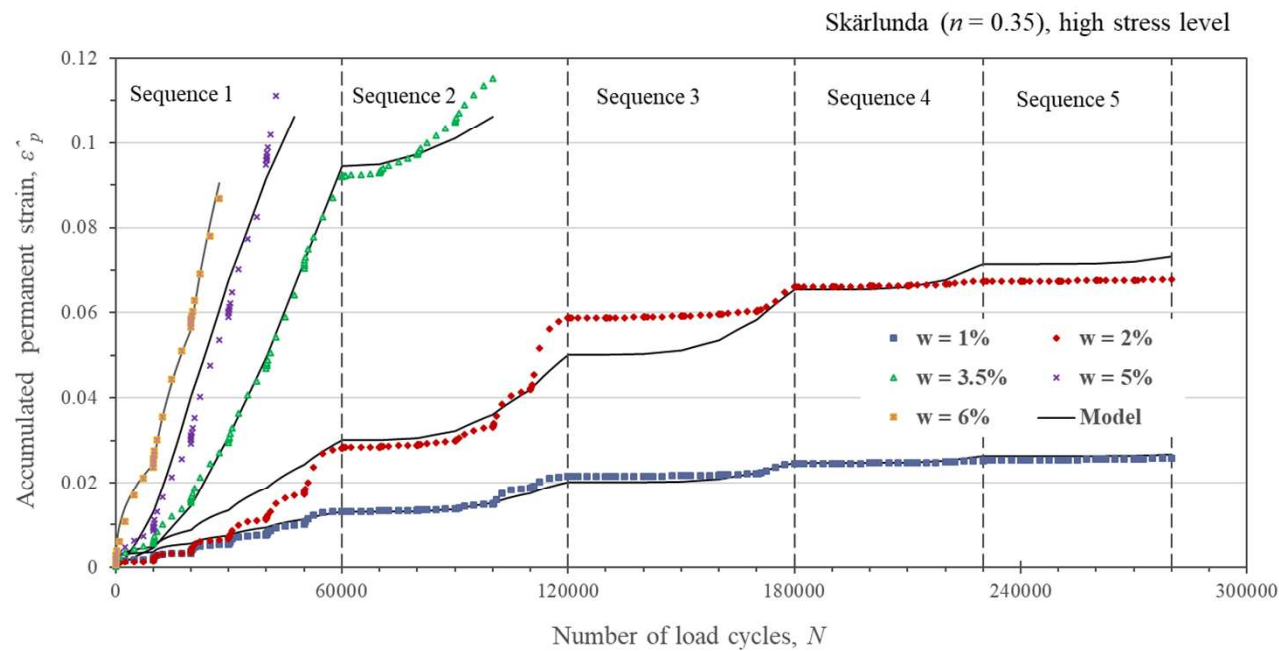


# Moisture impact on permanent deformation

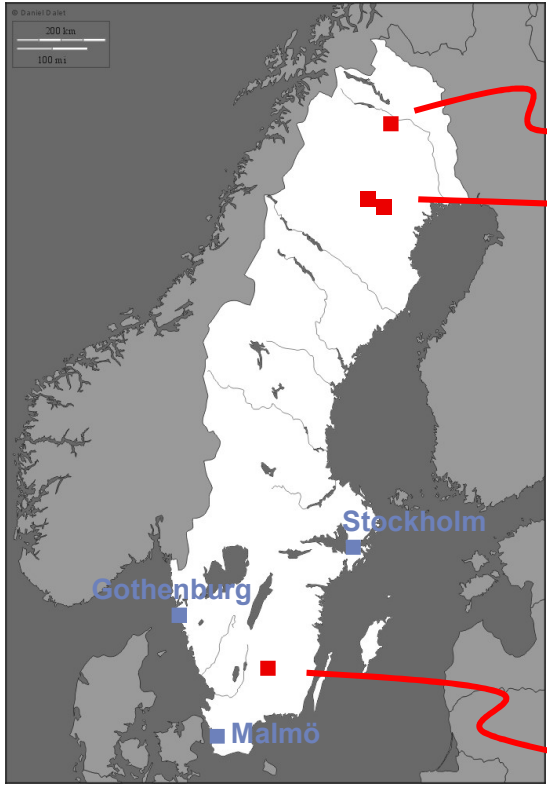
## Base course material

### Multi Stage (MS) approach

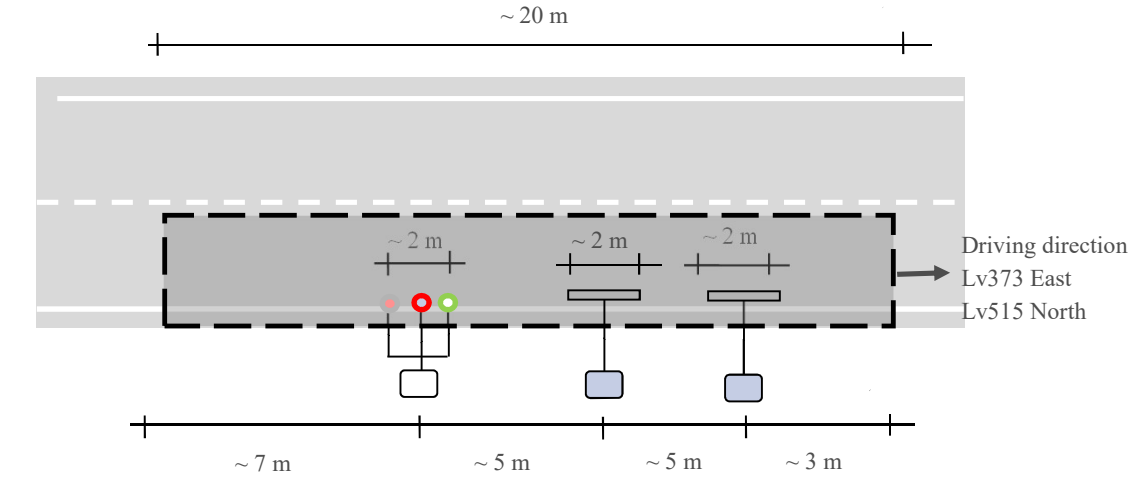
$$\hat{\epsilon}_p(N) = a \epsilon_r N^{b \epsilon_r} \quad a = a(w \text{ or } S_r)$$



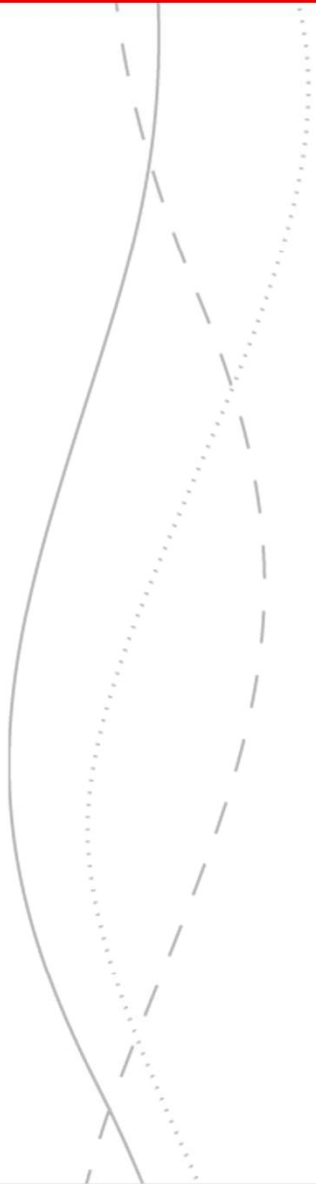
# Field Monitoring



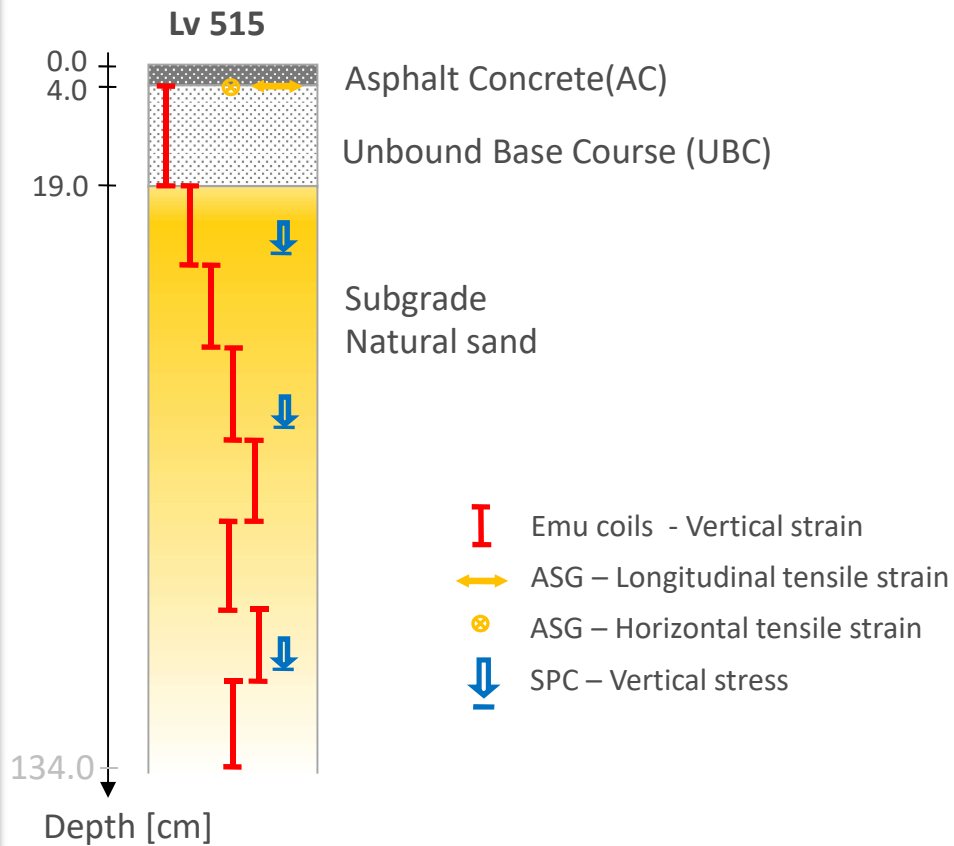
# Instrumentation #2



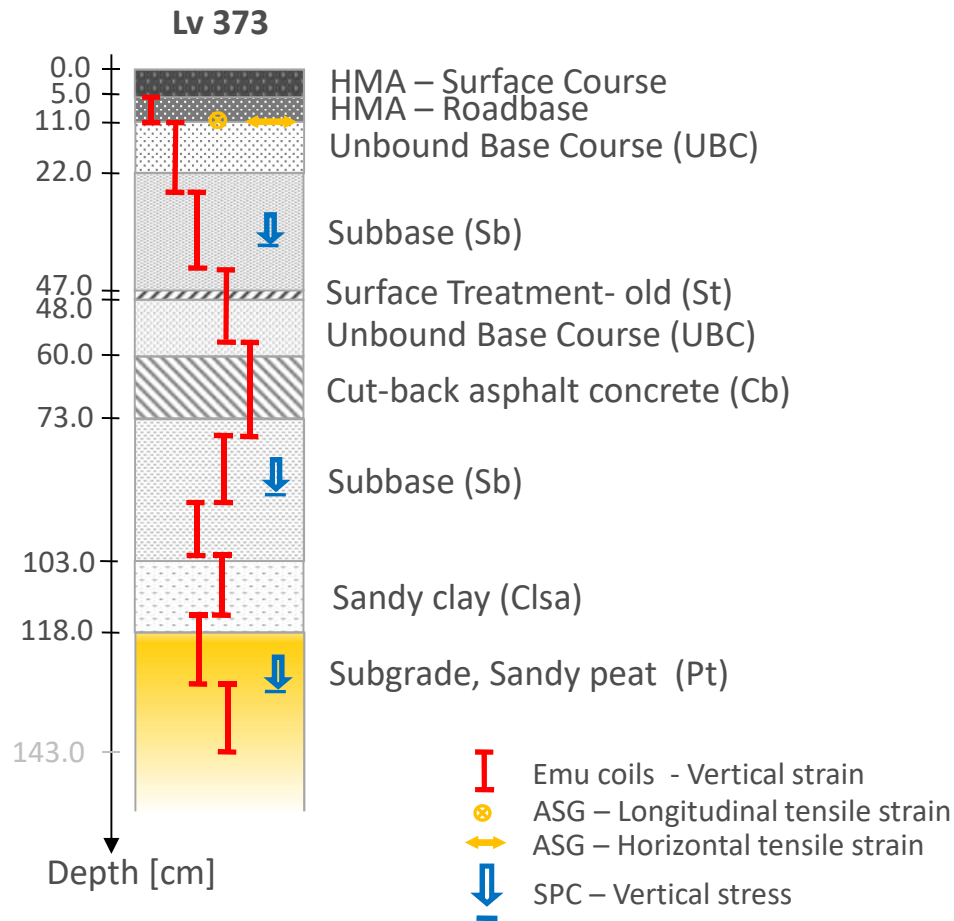
- Data acquisition, power supply, etc..
- Connection box
- Road instrumentation in outer wheel path
- Moisture rod
- Frost rod
- Temperature sensors in AC



# Instrumentation Lv515 - road response sensors



# Instrumentation Lv373 - road response sensors



# Testing campaigns



4 campaigns

August 2018

May 2019

June 2019

August 2019

In each campaign

FWD 30, 50 & 65 kN

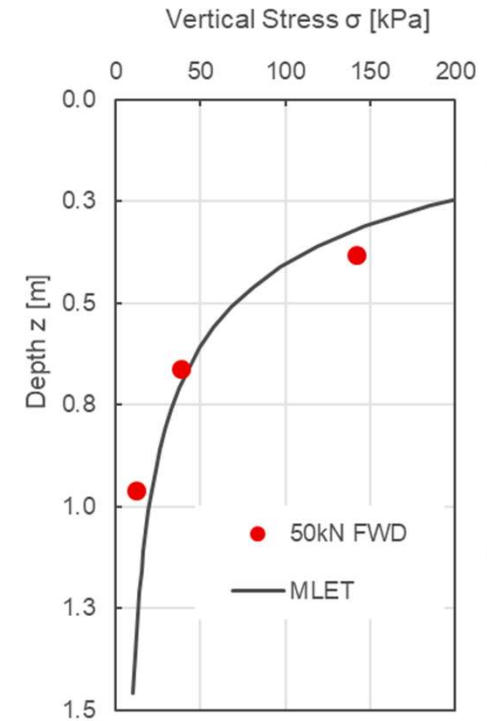
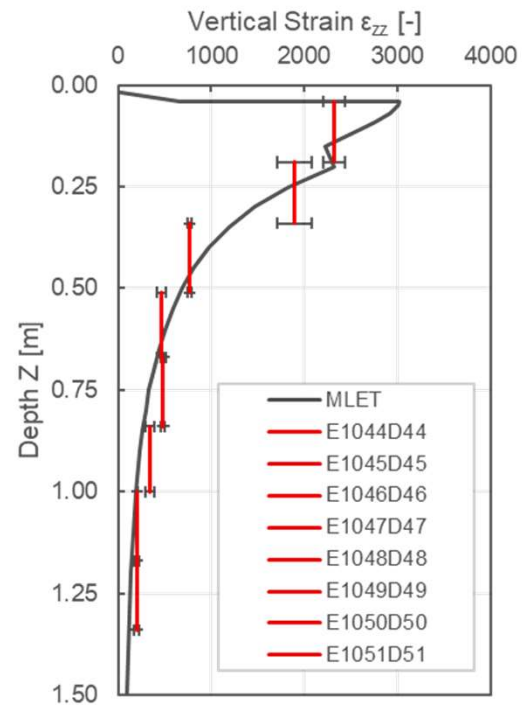
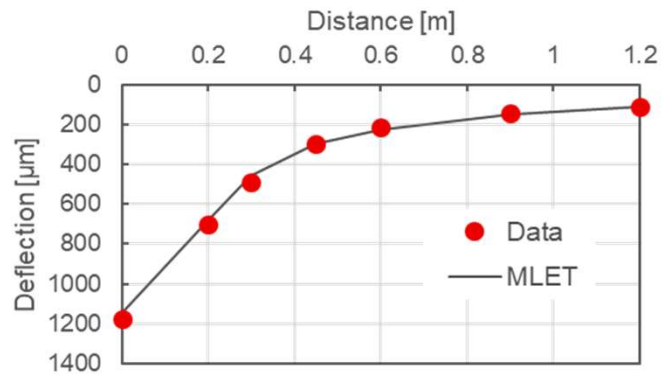
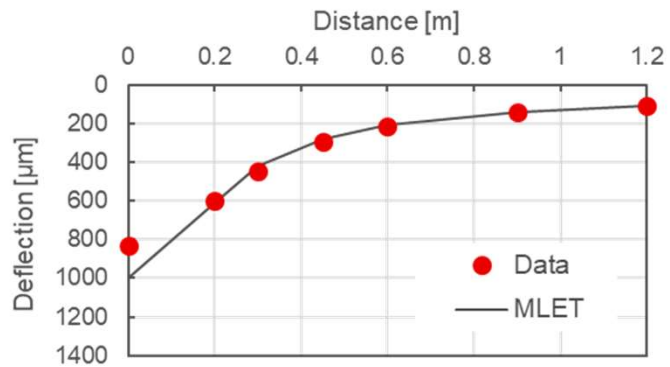
HV1 74 tonnes

HV2 64 tonnes

HV3 68 tonnes



# FWD measurements Lv515

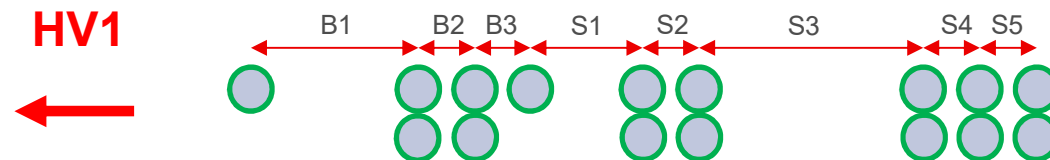


# Heavy Vehicle testing – HV1 (60 km/h)



HV1 74 t    August 2019 Lv515  
 1323  
 S TTS TT TTT

8.60 (840) = 8.60  
 8.75 (750) + 7.80 (750) + 6.15 (840) = 22.70  
 7.35 (850) + 7.25 (850) = 14.60  
 8.95 (850) + 9.30 (850) + 9.25 (850) = 27.50  
 73.40 t

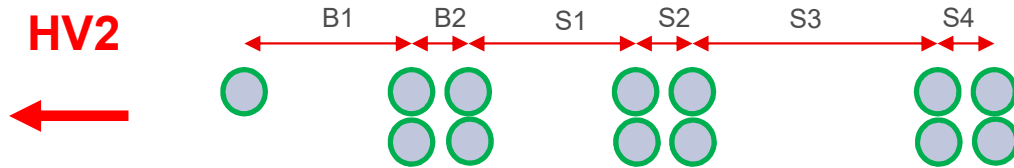


# Heavy Vehicle testing – HV2 (60 km/h)



HV2 64 t    August 2019 Lv515  
 1222  
 S TT TT TT

7.80 (940)	= 7.80
10.75 (660) + 9.90 (670)	= 20.65
7.10 (780) + 7.40 (770)	= 14.50
10.10 (810) + 10.30 (800)	= <u>20.40</u>
	<b>63.35 t</b>

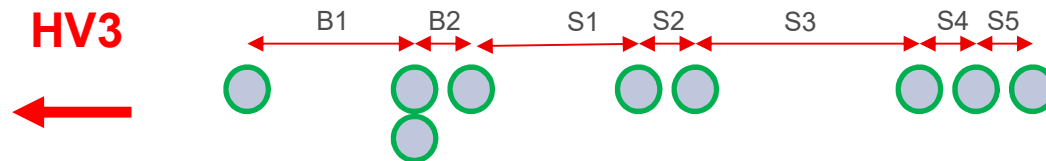


# Heavy Vehicle testing – HV3 (60 km/h)

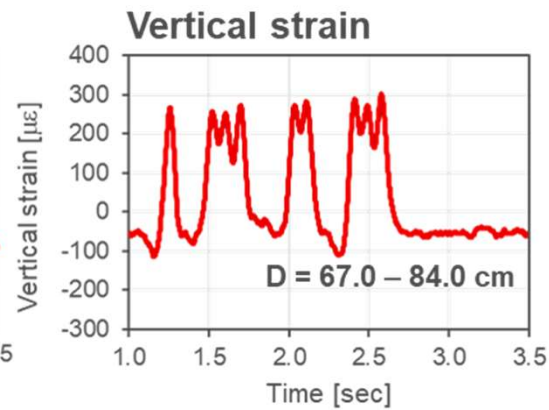
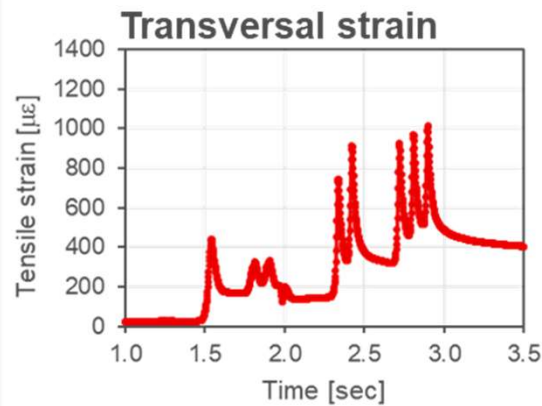
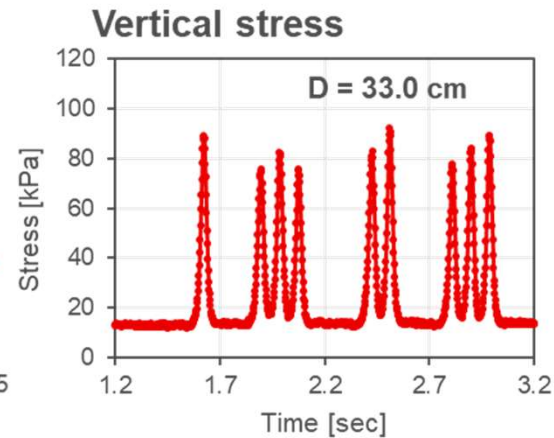
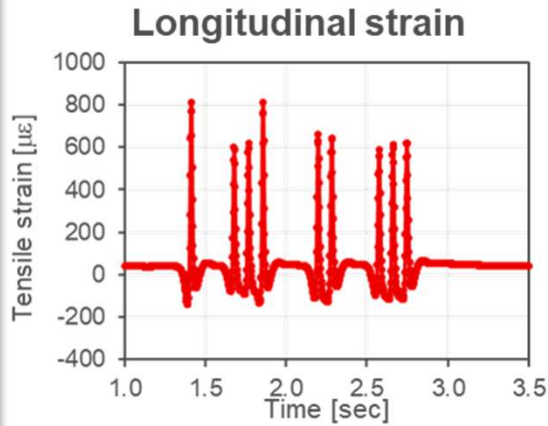


HV3 68 t August 2019 Lv515  
1223  
S TS SS SSS

9.40 (880) = 9.40  
 12.05 (800) + 7.75 (800) = 19.80  
 8.85 (810) + 9.90 (890) = 18.75  
 6.65 (850) + 7.35 (880) + 7.40 (850) = 21.40  
 69.35 t



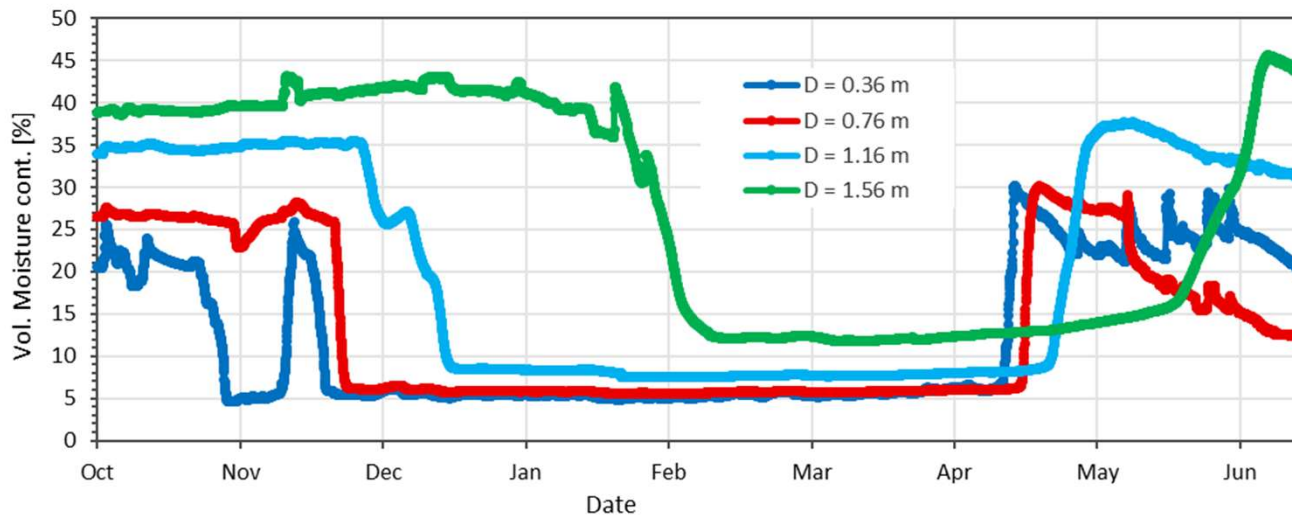
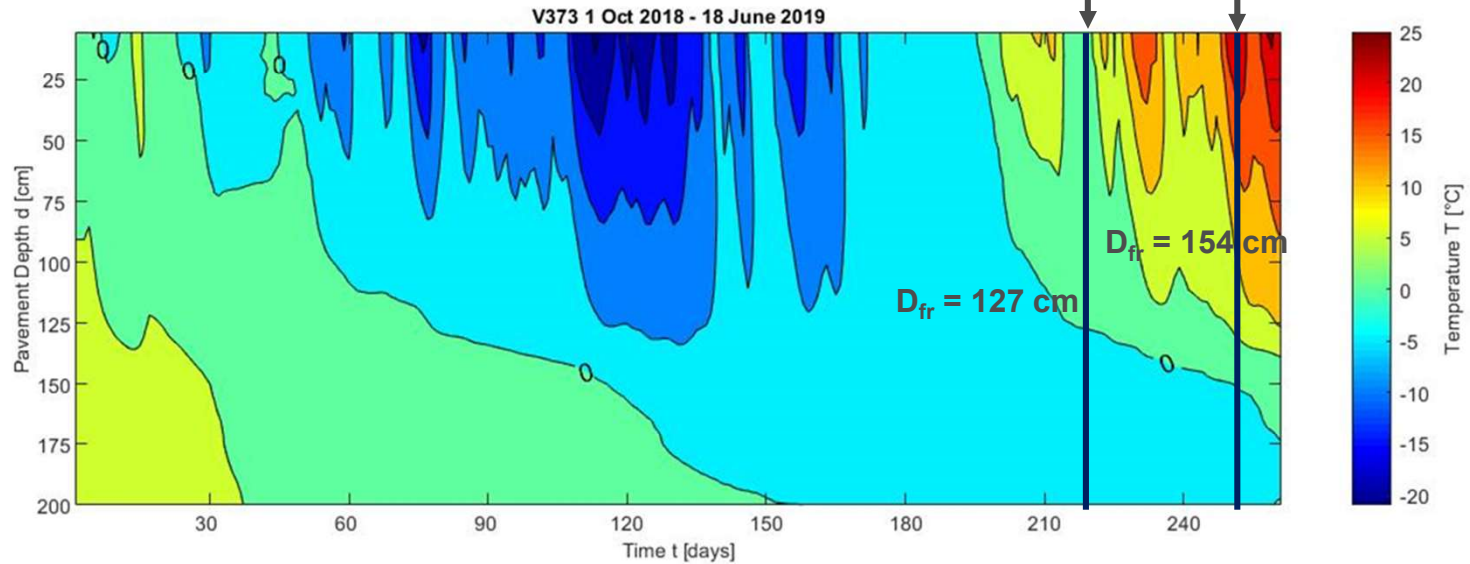
# Full scale testing – HV1 74 t: Measured response



# Långtresk – spring thaw 2019

7 May

10 June



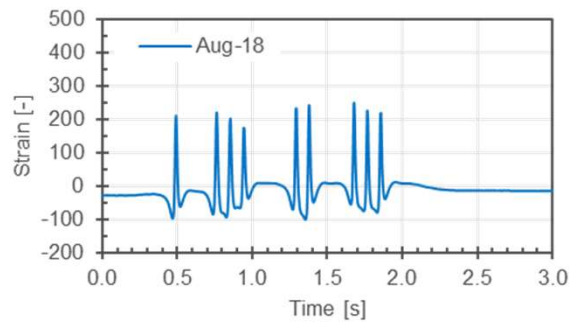
# Comparison – Measurements

## Lv373

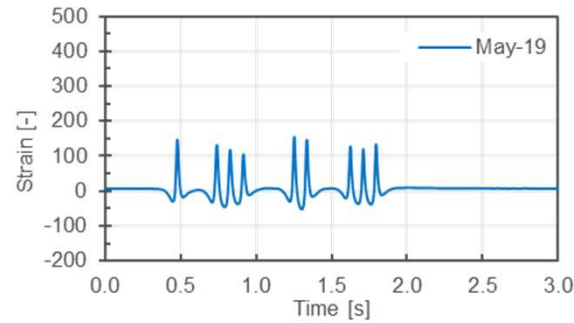


27.08.2018

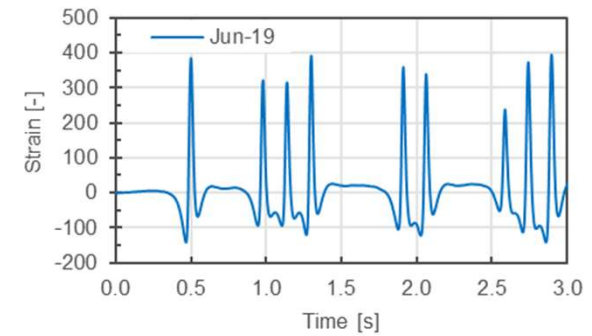
**Longitudinal strain:**



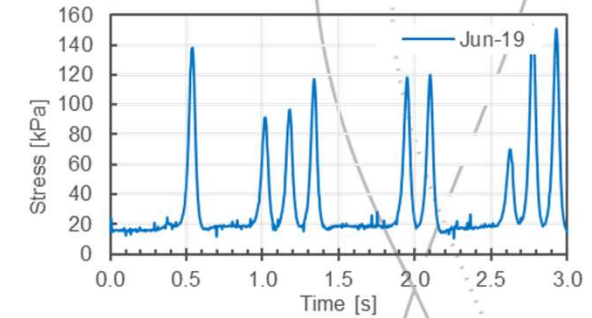
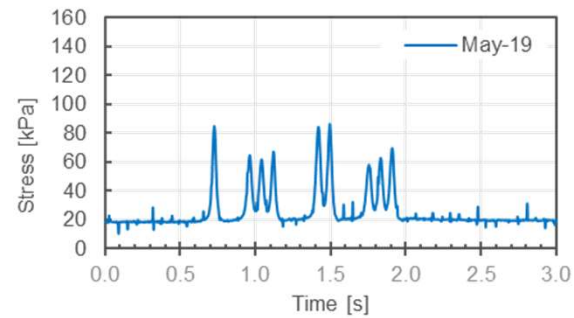
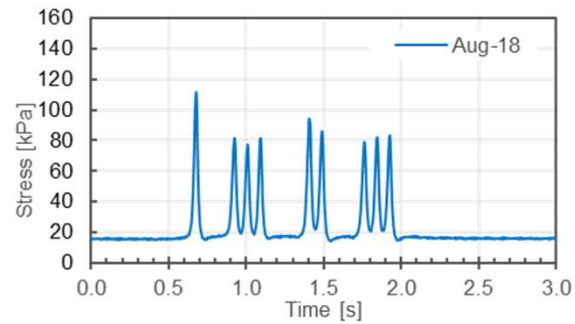
07.05.2019



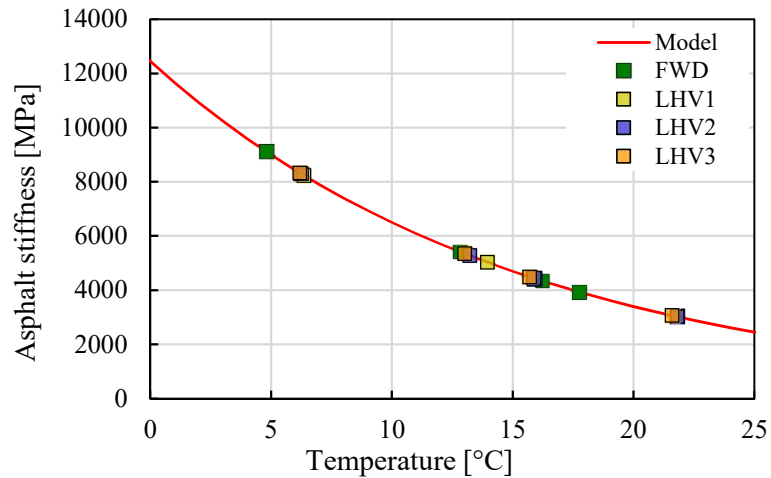
10.06.2019



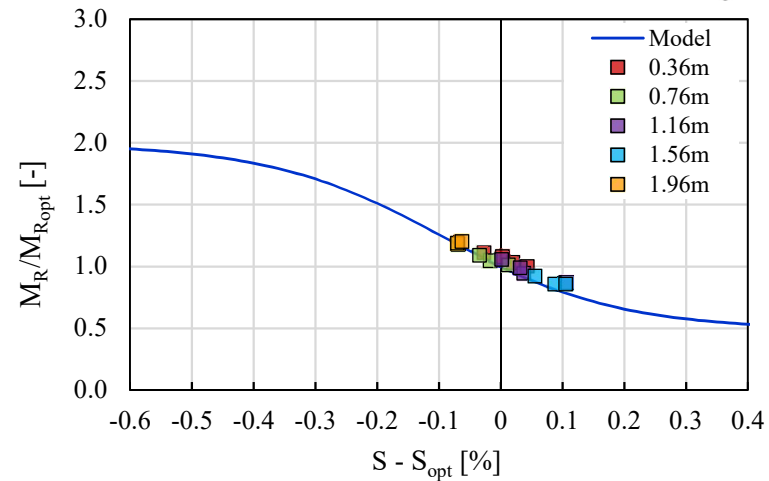
**Vertical stress:**



# Climate adjustments - Lv515



$$E_T = E_{T,ref} \cdot e^{-b(T-T_{ref})}$$



$$\log \frac{M_R}{M_{R,opt}} = a + \frac{b-a}{1 + \exp(\beta + k_s(S - S_{opt}))}$$

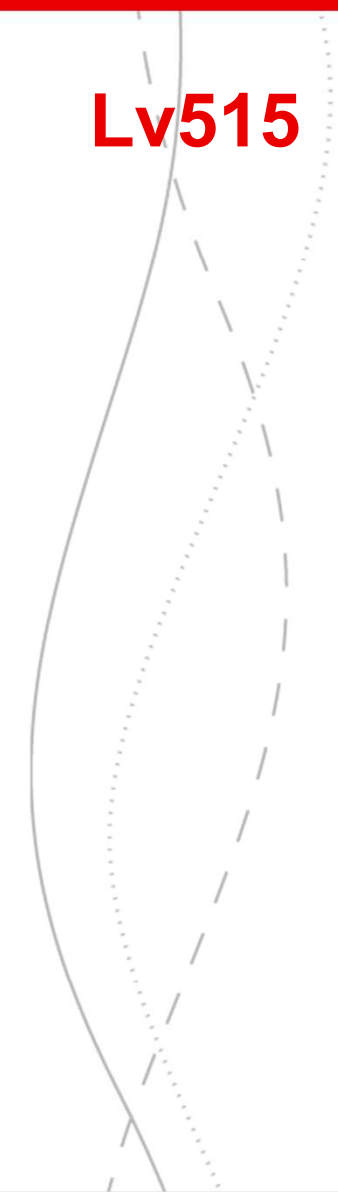
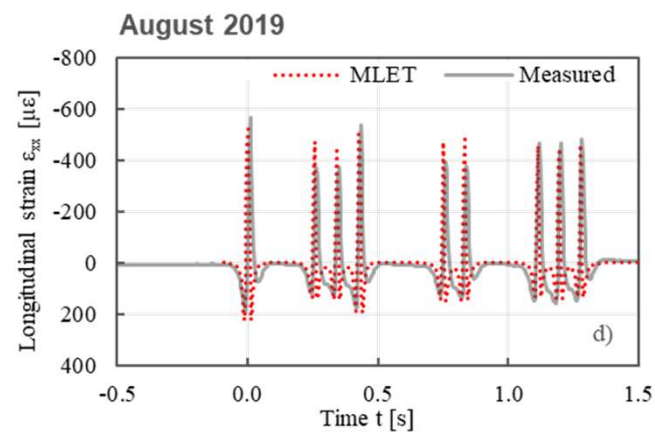
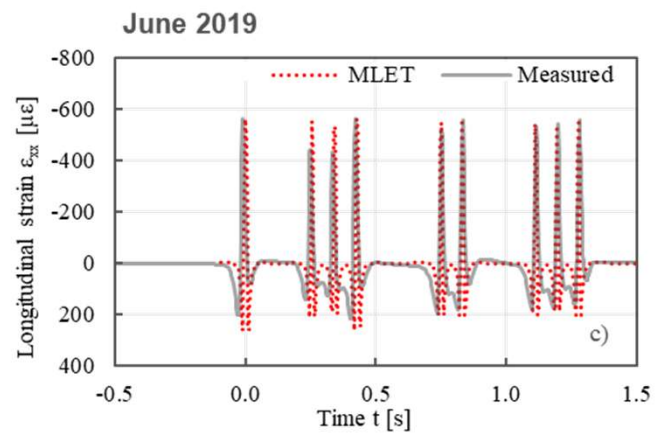
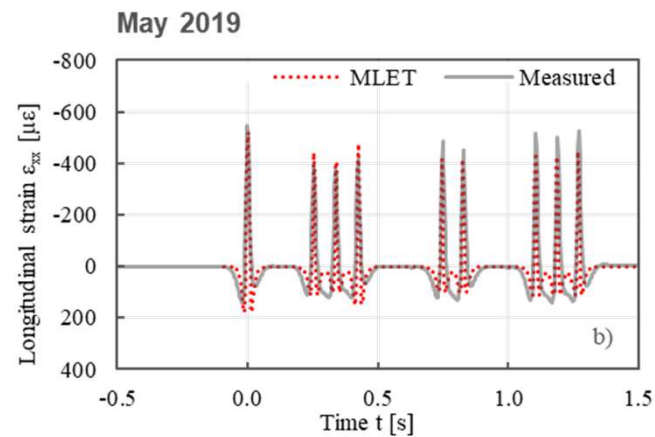
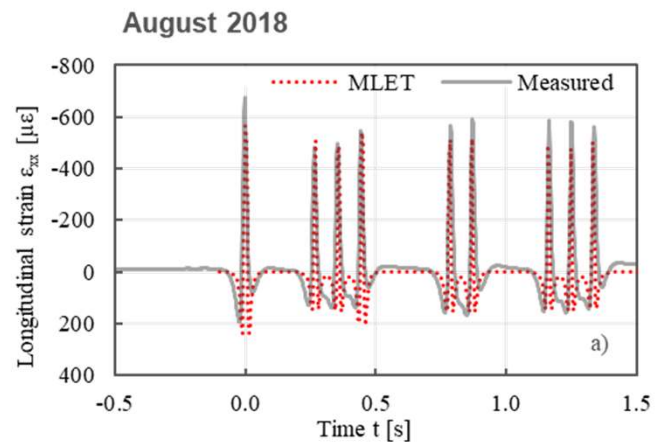


# Långtresk – Validation

HV1 - 74 ton

Lv515

## Longitudinal strain



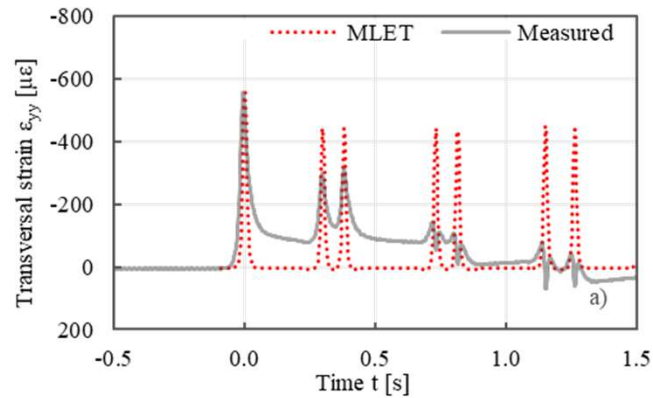
# Långtresk – Validation

HV2 - 64 ton

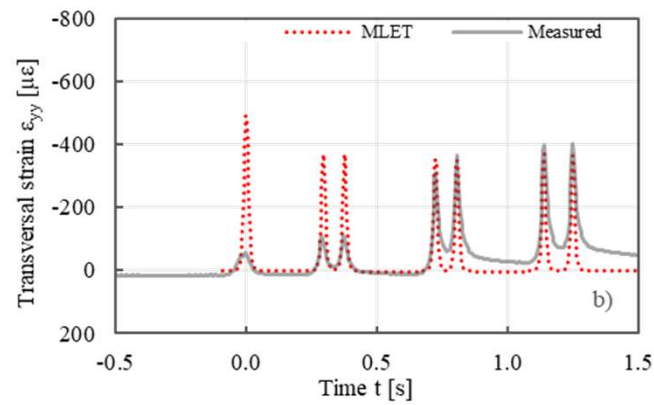
Lv515

## Transversal strain

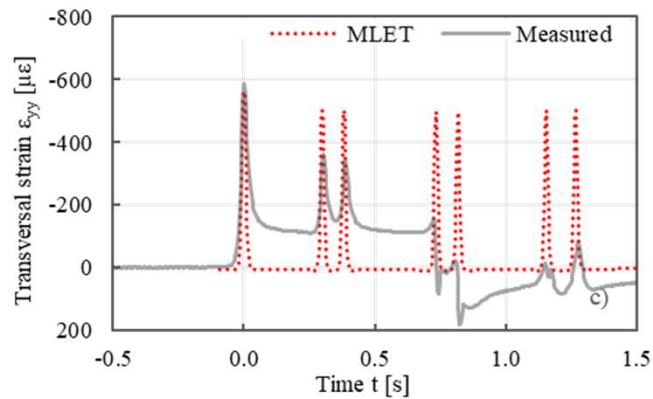
August 2018



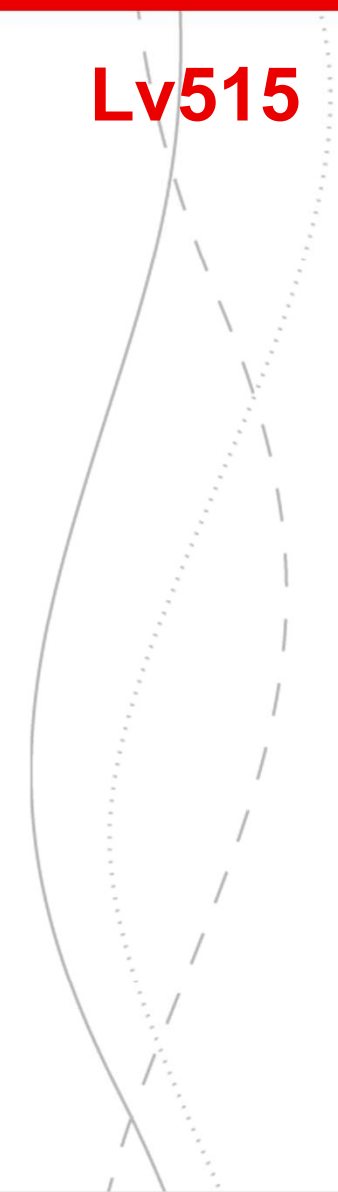
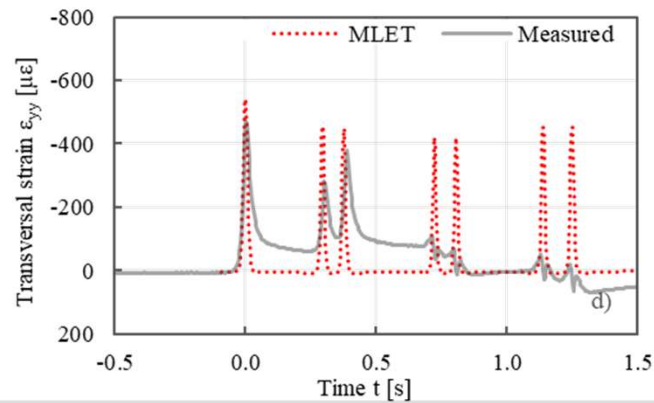
May 2019



June 2019



August 2019

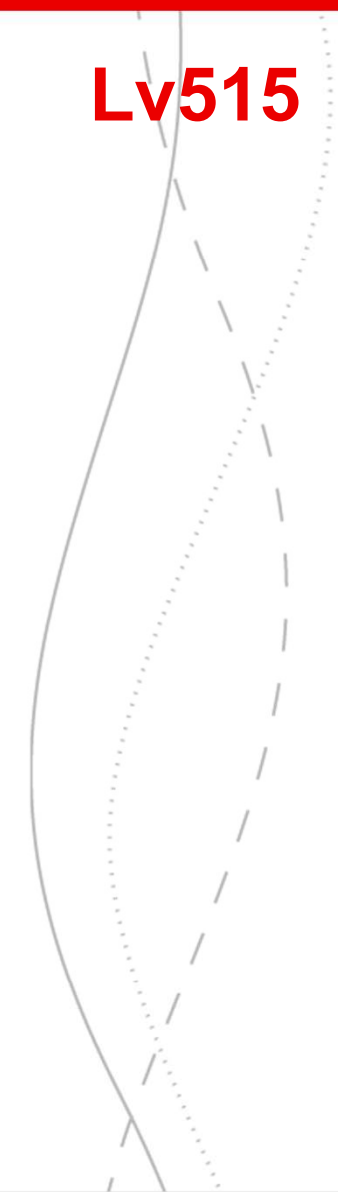
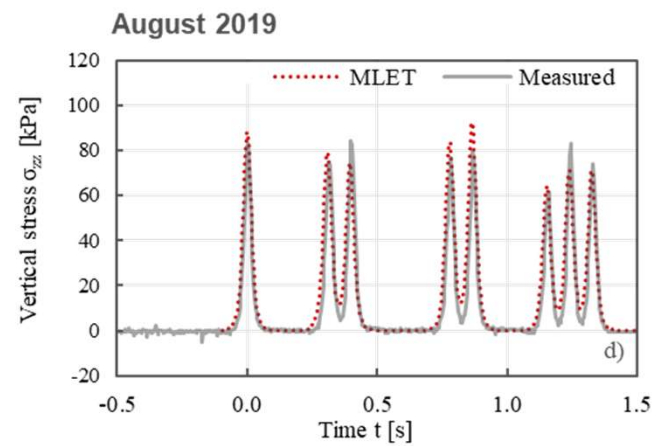
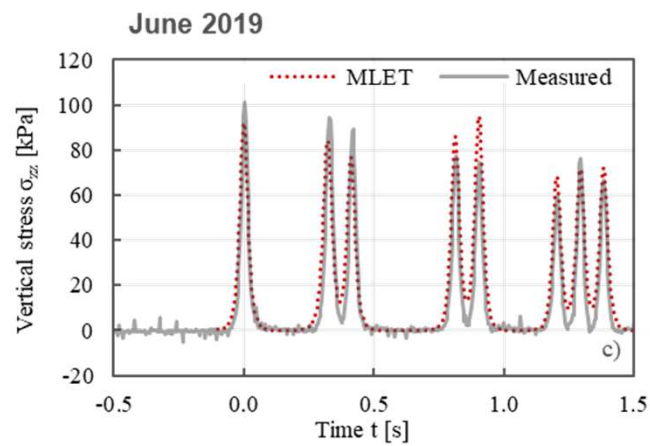
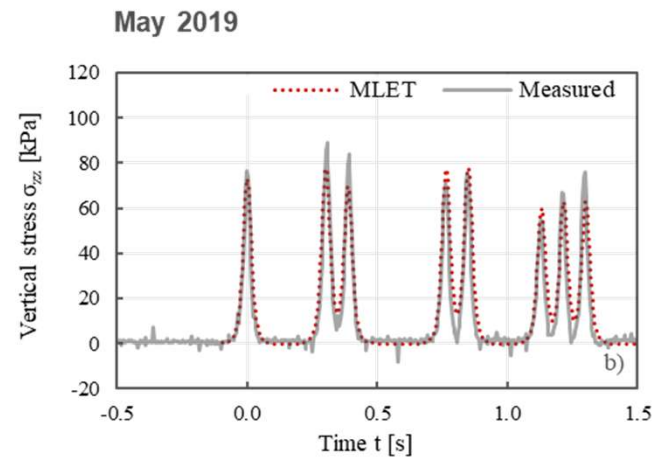
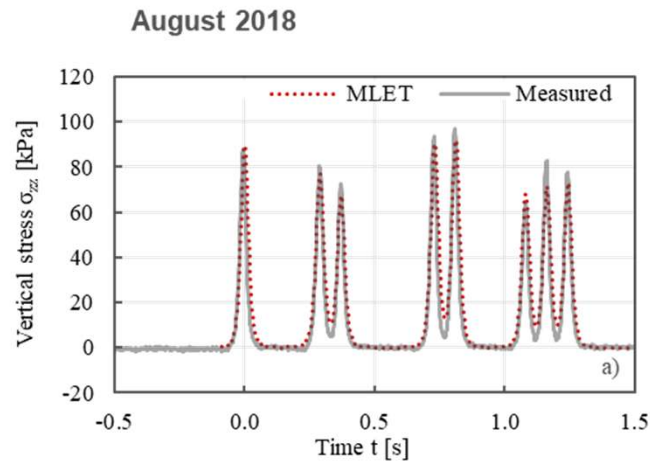


# Långtresk – Validation

HV3 - 68 ton

Lv515

## Vertical stress



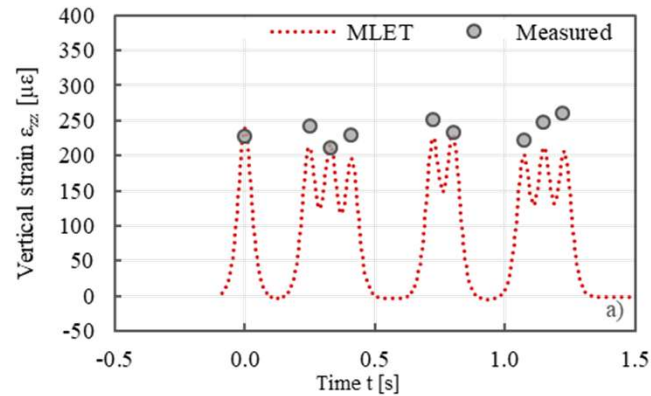
# Långtresk – Validation

## HV1 - 74 ton

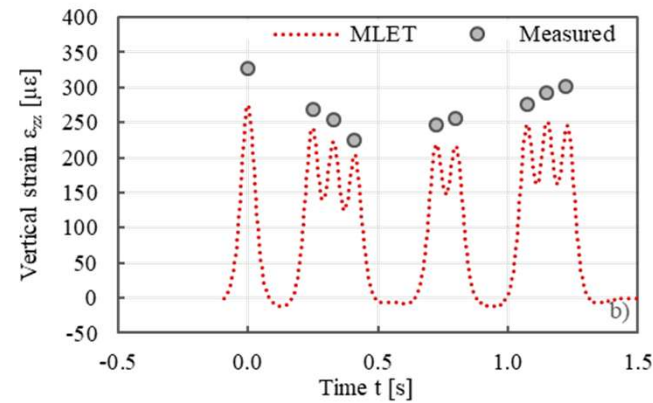
## Lv515

### Vertical strain

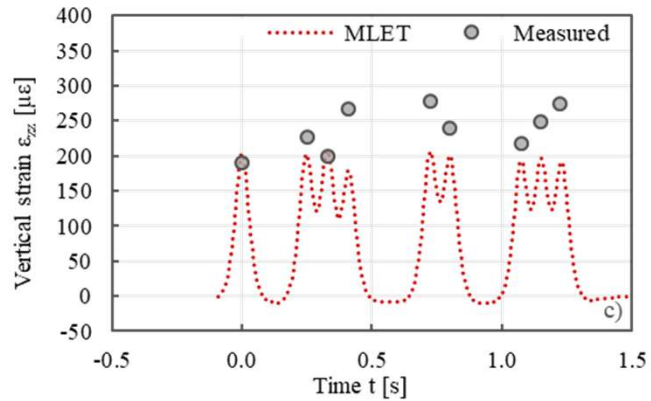
August 2018



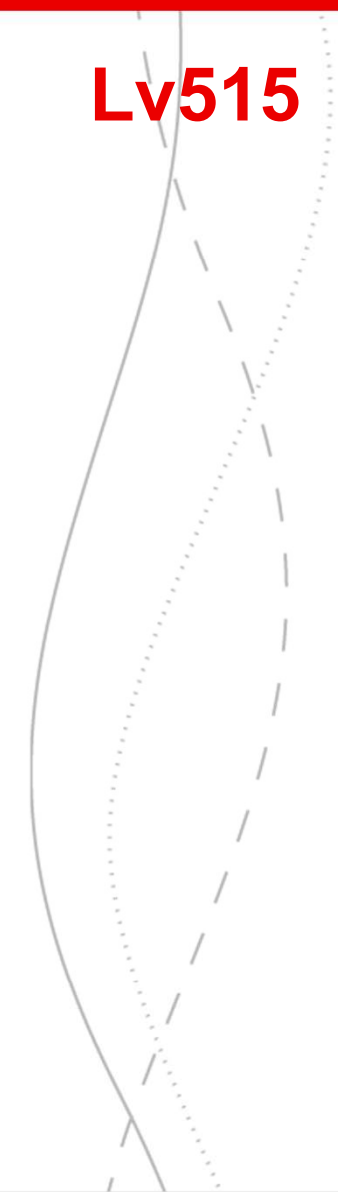
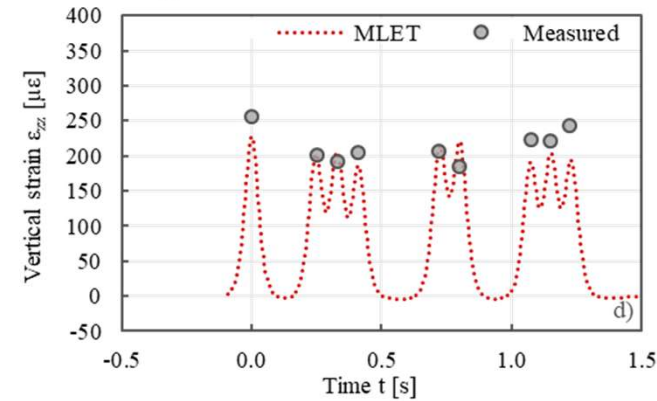
May 2019



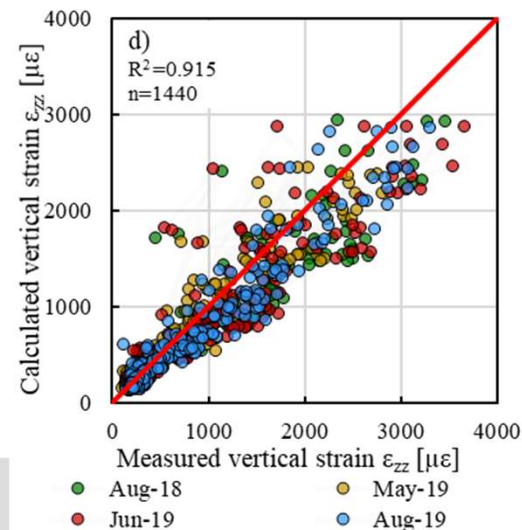
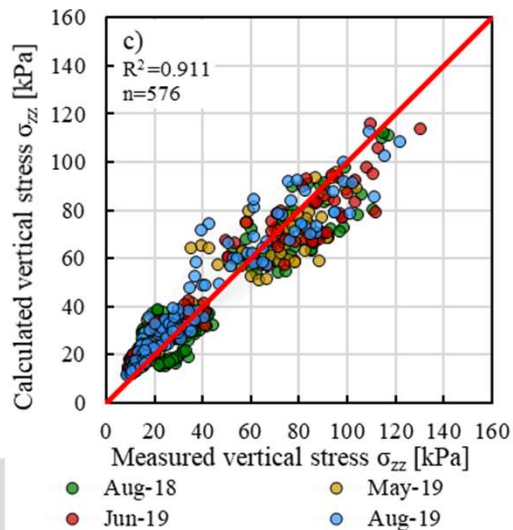
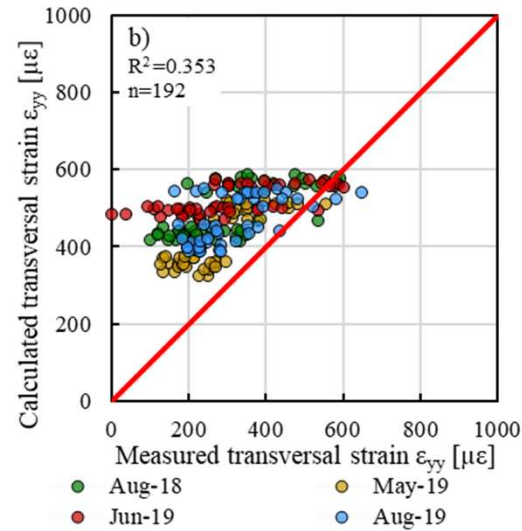
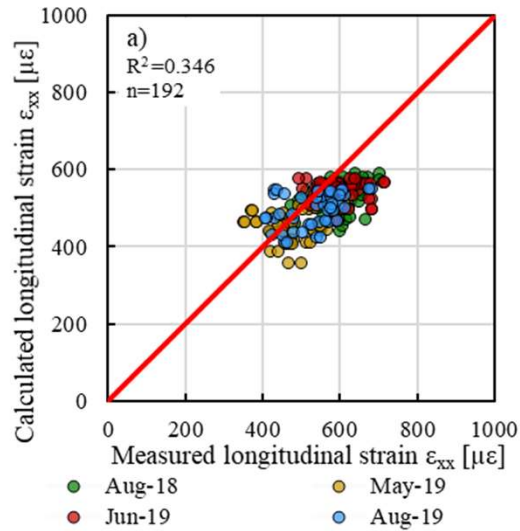
June 2019



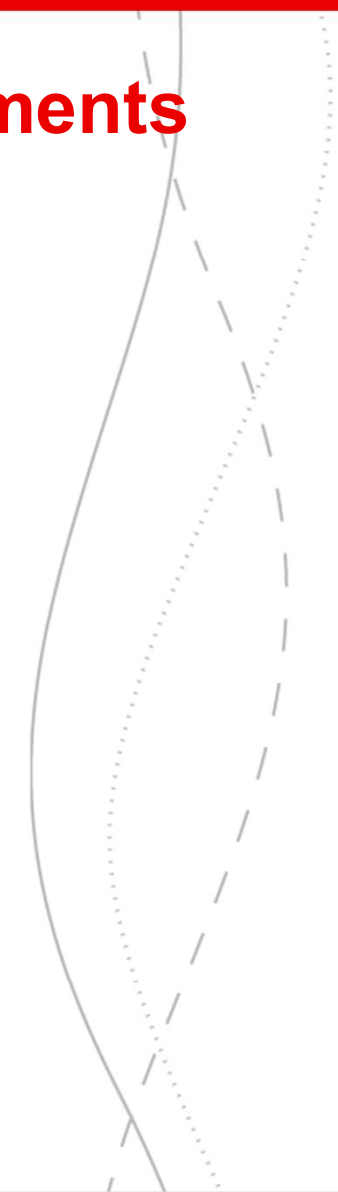
August 2019



# Validation: Calculation against measurements



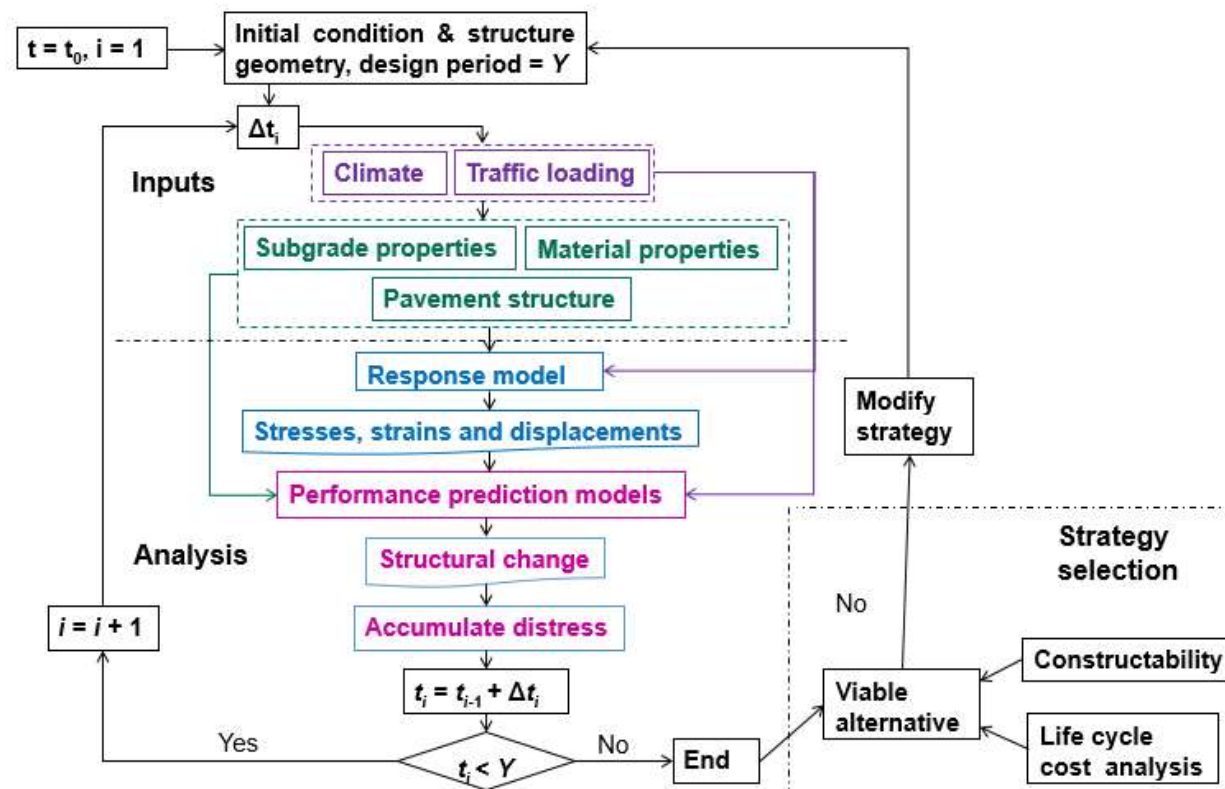
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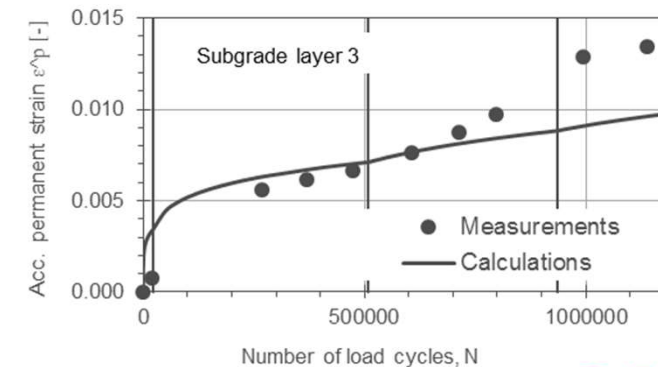
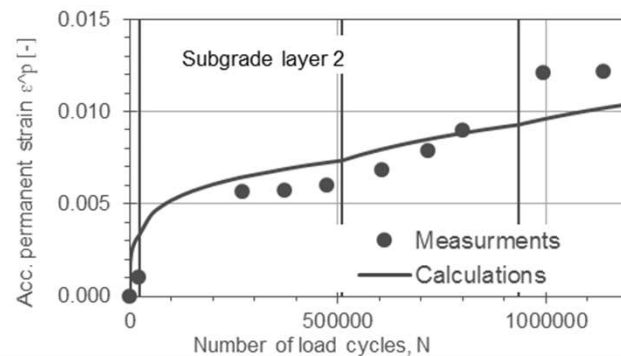
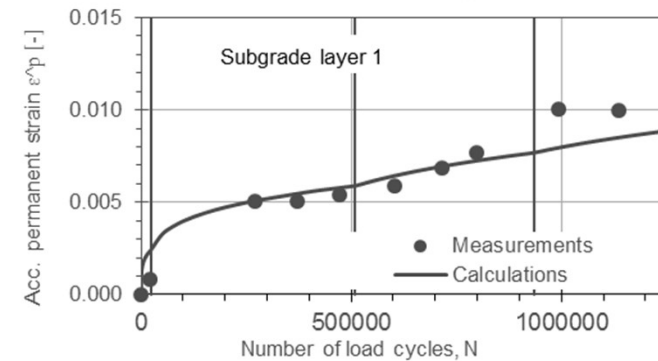
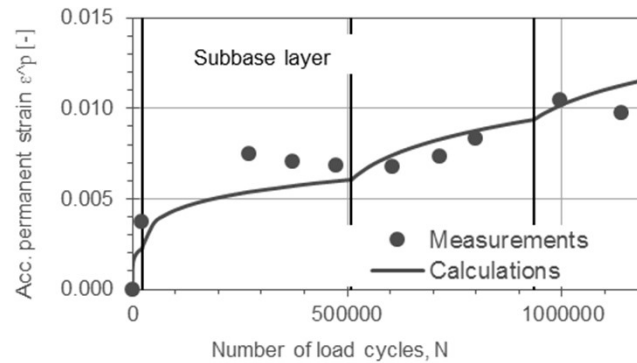
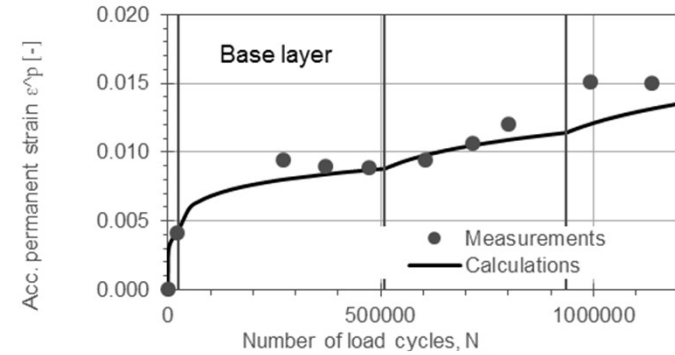
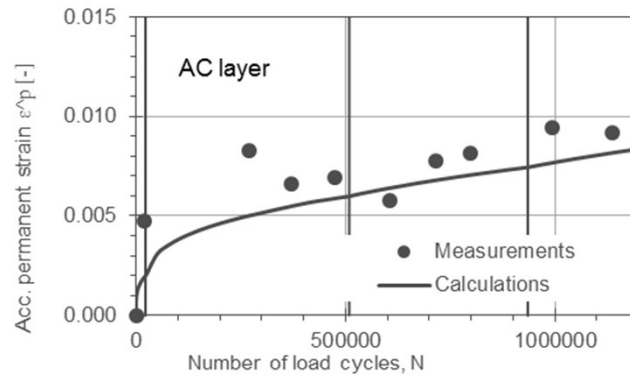
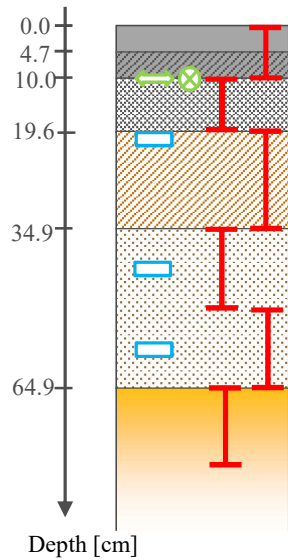
# M-E design

# ERAPave PP

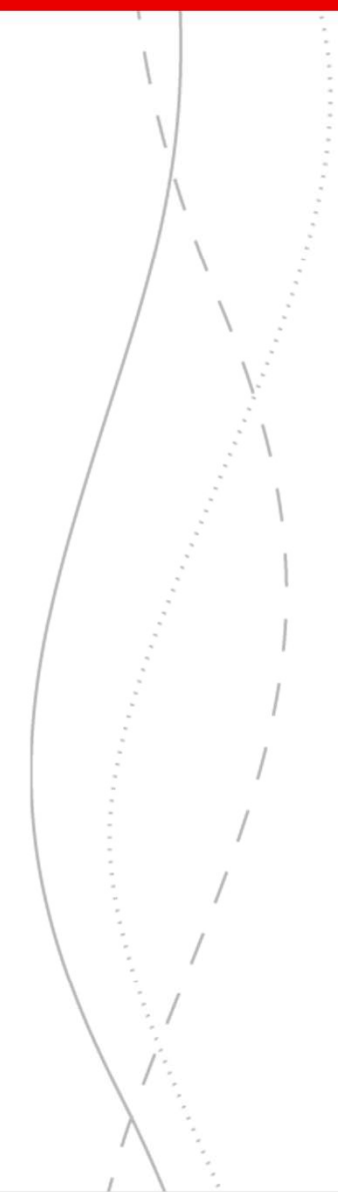
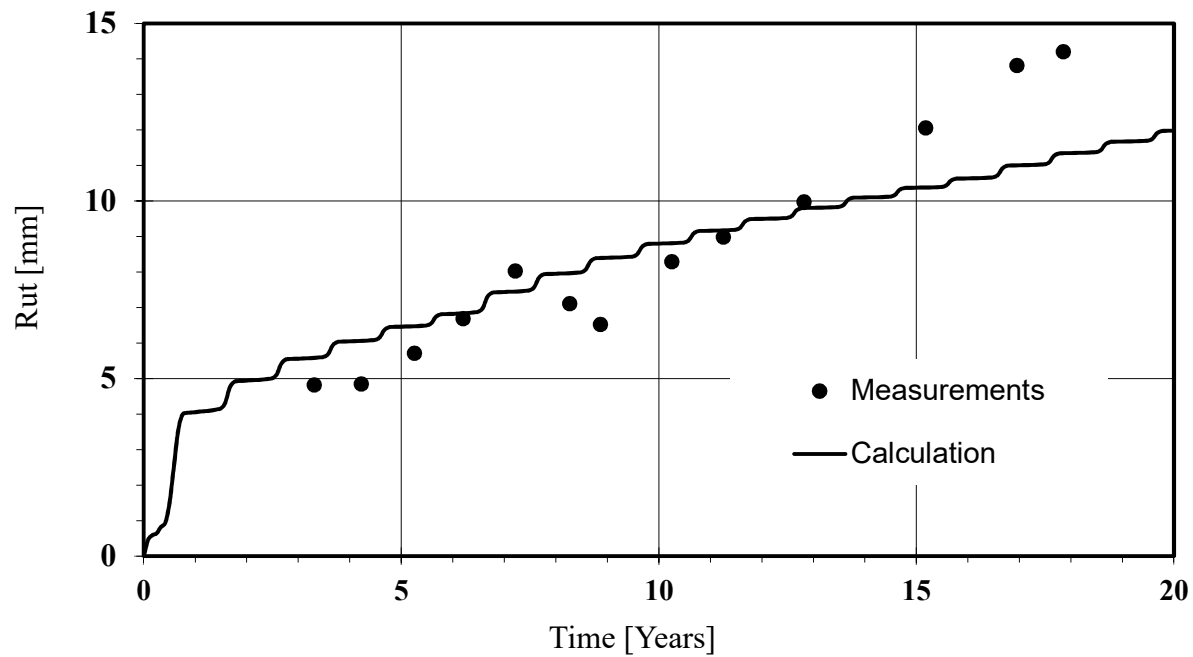
Overview of the M-E design and performance approach



# Calibration & Validation – APT testing



# LTTP road – Permanent deformation prediction Validation / Calibration





# Conclusions

Moisture content within the pavement structure changes due to climate condition. Moisture has a great impact on pavement unbound layers behaviour. This is true regarding:

- Stiffness characteristics

- Permanent deformation behaviour

This is evident from:

- Full-scale APT using an HVS in a climate controlled environment

- Controlled laboratory RLT tests

- Field monitoring programs using FWD to mimic the heavy axle loading

During spring thaw large increase in moisture content in UGM is frequently observed that affects the structural behaviour of the pavement structure. By updating the stiffness properties of the UGM layers with moisture content better agreement is gained between observations and calculations.

M-E based design and performance prediction scheme for thin pavements in seasonal areas is under development in Sweden.